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# Integrating thermal stress indexes within Shuttleworth–Wallace model for evapotranspiration mapping over a complex surface

Jamal Elfarkh<sup>1</sup> · Salah Er-Raki<sup>1,2</sup> · Jamal Ezzahar<sup>2,3</sup> · Abdelghani Chehbouni<sup>2,4</sup> · Bouchra Aithssaine<sup>2</sup> · Abdelhakim Amazirh<sup>2</sup> · Saïd Khabba<sup>2,5</sup> · Lionel Jarlan<sup>4</sup>

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## Abstract

The main goal of this work was to evaluate the potential of the Shuttleworth–Wallace (SW) model for mapping actual crop evapotranspiration (ET) over complex surface located in the foothill of the Atlas Mountain (Morocco). This model needs many input variables to compute soil ( $r_s^s$ ) and vegetation ( $r_s^v$ ) resistances, which are often difficult to estimate at large scale particularly soil moisture. In this study, a new approach to spatialize  $r_s^s$  and  $r_s^v$  based on two thermal-based proxy variables was proposed. Land Surface Temperature (LST) and Normalized Difference Vegetation Index (NDVI) derived from Landsat data were combined with the endmember temperatures for soil ( $T_{s_{\min}}$  and  $T_{s_{\max}}$ ) and vegetation ( $T_{v_{\min}}$  and  $T_{v_{\max}}$ ), which were simulated by a surface energy balance model, to compute the soil ( $T_s$ ) and the vegetation ( $T_v$ ) temperatures. Based on these temperatures, two thermal proxies ( $SI_{ss}$  for soil and  $SI_{sv}$  for vegetation) were calculated and related to  $r_s^s$  and  $r_s^v$ , with an empirical exponential relationship [with a correlation coefficient ( $R$ ) of about 0.6 and 0.5 for soil and vegetation, respectively]. The proposed approach was initially evaluated at a local scale, by comparing the results to observations by an eddy covariance system installed over an area planted with olive trees intercropped with wheat. In a second step, the new approach was applied over a large area which contains a mixed vegetation (tall and short) crossed by a river to derive  $r_s^s$  and  $r_s^v$ , and thereafter to estimate ET. A Large aperture scintillometer (LAS) installed over a line transect of 1.4 km and spanning the total area was used to validate the obtained ET. The comparison confirmed the ability of the proposed approach to provide satisfactory ET maps with an RMSE, bias and  $R^2$  equal to 0.08 mm/h, 0.06 mm/h and 0.80, respectively.

## Introduction

The fast-growing population and economy in recent decades are accompanied by an increase in agricultural production. Agricultural and irrigation techniques have been widely developed, but the deterioration and depletion of water resources remain a problem that threatens the future of food security, especially in arid and semi-arid zones (Plattner et al. 2009; Gohar et al. 2019). Rational management of water resources, which is a primary concern for the managers, requires a good knowledge of the water and energy processes taking place in the soil-vegetation-atmosphere continuum (Blinda 2012; Bhattarai et al. 2019). Indeed, the control of these processes allows to assess the exact amount of water that the plant requires overtime, which is similar to the field water loss through evapotranspiration (Allen et al. 2011). The process of evapotranspiration is difficult to determine because of various challenges, including the vegetation complexity, plant diversity, lack of available data and because the in-situ direct measurement of ET is difficult

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in complex surfaces like our study site. Then an accurate assessment of evapotranspiration (ET) is crucially needed at the basin scale for studying the hydrological processes and water balance especially from upstream to downstream and it is required for a good integrated water management. There is thus an imperative need to develop reliable computation method with a limited number of input parameters especially over complex surfaces.

Several methods have been used to measure ET and its components [plant transpiration (T) and soil evaporation (E)], which are different in complexity and/or in accuracy. The principles of these methods are various; they can be hydrological, physiological or micrometeorological. Based on the hydrological balance, the lysimeter provides direct evaporation or evapotranspiration measurements at a local scale and over homogeneous canopy (Allen et al. 2011; Sánchez et al. 2019). To assess the plant transpiration, the physiological approach has been used based on introducing a source of low-grade heat into the stem or the trunk of a plant. This approach known as the sap flow method, can be used in homogeneous crops but it requires an up-scaling procedures to extrapolate measurements from individual plants to the stand level transpiration (Green et al. 2003; Steppe et al. 2010; Er-Raki et al. 2010a; Rafi et al. 2019). Currently, around the world the micrometeorological techniques such as eddy covariance are widely used to measure ET over a scale of a few hectares, depending on the height of the measurements (Ezzahar et al. 2007; Allen et al. 2011; Fang et al. 2020). By contrast, the scintillometer technique that was recently developed allows for measurements of sensible (optical LAS) and latent (microwave LAS) heat fluxes over transects up to 10 km (Ezzahar and Chehbouni 2009; Ezzahar et al. 2009b, a; Zieliński et al. 2013, 2017; Yee et al. 2015). In addition, scintillometers are easy to install, to monitor and can provide measurements of the surface fluxes over complex surfaces which makes them suitable for validating remote sensing-based methods (Duchemin et al. 2008; Tang and Li 2015; Huang et al. 2016; Ait Hssaine et al. 2018; Saadi et al. 2018). The LAS applies the Monin–Obukhov Similarity Theory (MOST) to estimate the sensible heat flux. However, the applicability of MOST is limited when conditions are not favorable, which can happen for a number of reasons. Atmospheric conditions, instrumental setup, data processing and evaluation criteria (particularly choice of similarity function and variable of interest) can all affect the MOST applicability (Ward 2017).

With regard to modelling aspect, there are different types of models to estimate surface fluxes. They range from complex physically based, conceptual, to empirical ones. There are some models characterised by a simplified relation using thermal infrared and micrometeorological data (Jackson et al. 1977; Seguin and Itier 1983). Others are based on residual methods of the energy budget (Surface Energy

Balance Algorithm for Land (Bastiaanssen et al. 1998), Surface Energy Balance System (Su 2002), two-source energy balance (Norman et al. 1995), Mapping Evapotranspiration at a high-Resolution with Internalized Calibration (Allen et al. 2007)). A third one, more complex, characterizes the energy and water transfers in all the continuum soil-vegetation-atmosphere (Interaction Soil Biosphere Atmosphere (Noilhan and Mahfouf 1996; Aouade et al. 2020), Simple Soil-Plant-Atmosphere Transfer (Braud et al. 1995), Soil Plant Atmosphere and Remote Sensing Evapotranspiration (Boulet et al. 2015) and the Interactive Canopy Radiation Exchange (Gentine et al. 2007)). Compared to those based only on the energy budget, this category of models needs more input data which is often not available at large scale. Finally, some other approaches use a crop coefficient to provide actual ET from reference or potential one (Allen et al. 2005; Neale et al. 2005). These models can be extended to large areas when they are combined with remote sensing data (Duchemin et al. 2008; Er-Raki et al. 2010b; Diarra et al. 2017). Satellite products such as land surface temperature (LST), emissivity, albedo and vegetation indexes have been improving in their spatiotemporal resolution during the recent years, especially with the launch of Landsat 7 and 8 and Sentinel 2 satellites. Consequently, mapping and assessing ET over heterogeneous and large areas became a promising challenge which has been largely investigated in recent years (Albergel 2010; Singh et al. 2014; Semmens et al. 2016; Tan et al. 2019).

The two components of the ET are influenced differently by many factors which mean that the contribution of each one (E and T) to the total ecosystem ET is highly variable in time and space (Aouade et al. 2016). Consequently, estimating accurate ET over vegetation canopy using two-source models is necessary since this type of model computes each component distinctly. In this context, Shuttleworth and Wallace developed in Shuttleworth and Wallace 1985 a two-source model taking into account the interaction flux from vegetation and soil separately. It is characterized by a rigorous physically based framework which provides accurate ET estimation values especially for row crops (Ortega-Farias et al. 2007; Zhang et al. 2008). However, Shuttleworth–Wallace (SW) model is significantly sensitive to errors in the values of soil and vegetation resistances (Zhu et al. 2014). These resistances can be parameterized using measurements of E, T and ET (Samanta et al. 2007; Villagarcía et al. 2010; Zhu et al. 2014). Many authors have used empirical equations to compute these resistances based on surface and root-zone soil water content (Ramírez et al. 2007; Were et al. 2007). However, the soil water content is difficult to obtain at a large scale. Several methods were developed to estimate this variable but they are complex and need the knowledge of many physical soil parameters (Guswa et al. 2002; Verhoef et al. 2006; Merlin et al. 2016). For this reason and to

149 estimate spatial values of ET using the SW model, a param-  
 150 eterization of the soil and vegetation resistances using a thermal-based proxy derived from Landsat was proposed in this  
 151 paper. The stress indexes presented by this proxy reflect the  
 152 hydric state of both soil and vegetation since the temperature  
 153 variation of the soil or the vegetation can be attributed to  
 154 change in the water content between dry and wet conditions.  
 155 In this context, good results have been obtained by relating  
 156 thermal-based proxy of vegetation water stress to canopy  
 157 resistance (Amazirh et al. 2017) and to stress coefficient in  
 158 FAO-56 (Olivera-Guerra et al. 2018, 2020). The novelty of  
 159 the proposed approach is the link of both vegetation and  
 160 soil resistances to the stress indexes which can provide an  
 161 accurate estimation of spatial ET.

163 This paper is organized as follows: first, an overview of  
 164 the study area, the experimental design and the proposed  
 165 approach is presented. After, a description of the obtained  
 166 results at a local scale is provided. Then, an illustration of  
 167 the spatial results with a discussion about the potential of  
 168 the developed approach to assessing the evapotranspiration  
 169 over a heterogeneous semi-arid region is presented. Finally,  
 170 a summary and conclusions are provided.

## 171 Materials and methods

### 172 Study area and data description

#### 173 Study area description

174 An experiment was conducted over the piedmont of the  
 175 Atlas mountain in the center of Morocco (Tahanaout city,  
 176 Fig. 1). This area is characterized by a semi-arid climate  
 177 with a low annual rainfall amount especially for 2017 where  
 178 an annual cumulative value of about 157 mm compared to  
 179 the cumulative value during last two decades (302 mm).  
 180 The land use mapping of the experimental area is also pre-  
 181 sented in Fig. 1a. According to this figure, one can remark  
 182 clearly that the area is heterogeneous and composed of small  
 183 fields planted by olive trees with a height ranging from 3 to  
 184 12 m which were measured using the 45° Triangle method  
 185 (Fig. 1b). Note that some farmers mix the olive trees with  
 186 herbaceous crops such as wheat, alfalfa and/or corn. In the  
 187 same area apricot, plum, orange and peach trees are also  
 188 cultivated. The bare soil is mainly present on the sides of  
 189 Rherhaya river and on the North-West part of the study area.  
 190 Additionally, the heterogeneity of the site is amplified by the  
 191 difference in the height between different trees and herba-  
 192 ceous crops. All fields are irrigated using the flooding tech-  
 193 nique. In general, the irrigation water comes from mountain  
 194 (rainfall or melting snow) and is diverted to the study area  
 195 through traditional networks (Bouimouass et al. 2020).

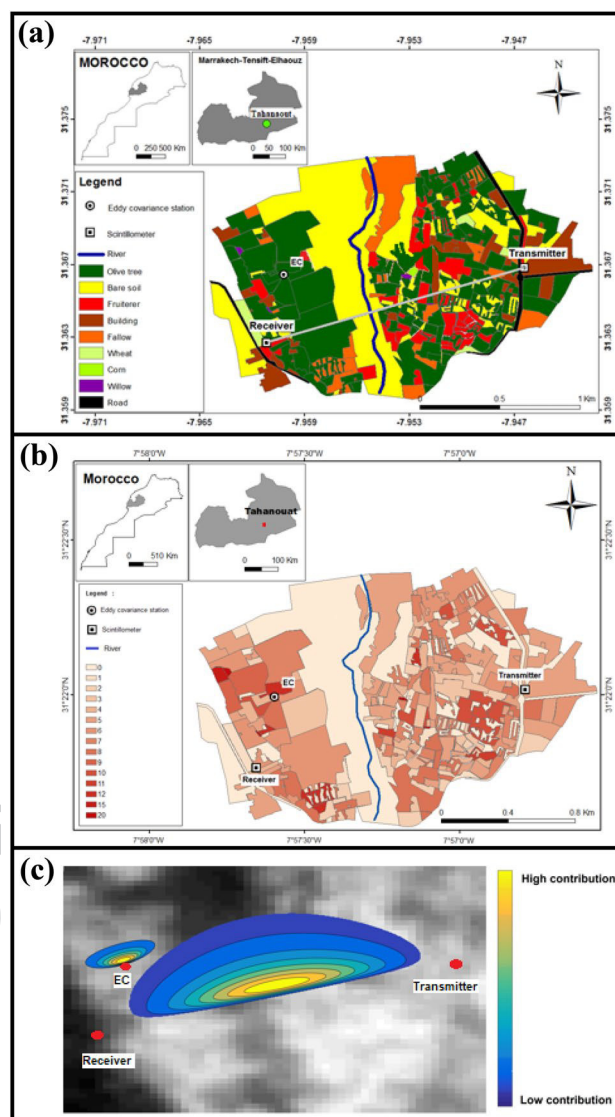


Fig. 1 Locations of the Eddy Covariance (EC) station, the scintillometer (transmitter and receiver) superimposed on the land use map (a), vegetation height map (b) and Landsat image with their footprint (c)

### 196 Meteorological data, eddy covariance and scintillometer 197 measurements

198 A set of instruments was deployed over the EC tower in the  
 199 study site for measuring meteorological data, turbulent  
 200 fluxes, soil moisture and surface temperature. Air tempera-  
 201 ture and humidity were measured with a Vaisala (HMP155,  
 202 Campbell scientific) at a height of about 15.6 m. The four  
 203 components of the net radiation were measured using a  
 204 CNR4 radiometer (Campbell scientific) at a height of about  
 205 16.7 m. The soil heat flux was averaged using the measure-  
 206 ment of two heat flux plates at 5 cm depths (HPF01, Hukse-  
 207 flux) in two locations: one below the tree (always shaded)  
 208 and the other between the trees (directly exposed to solar

radiation). Soil moisture was measured at different depths (5 and 15 cm) using CS655 water content reflectometers (Campbell Scientific). Radiometric brightness temperature was measured over the soil and the vegetation separately using an Infra-Red radiometer (IRTS-P's, Apogee) and then converted to land surface temperature (LST) using surface emissivity. One of the radiometers was positioned at height of about 11.7 m directed vertically towards the ground and the other one was positioned at height of about 6.5 m directed towards the vegetation with a view angle of about 60 degrees. An eddy covariance (EC) system was installed on 17.5 m height tower to measure the latent and sensible heat fluxes. It is composed of a three-dimensional sonic anemometer (CSAT3, Campbell Scientific Ltd.) and a Krypton hygrometer (KH20, Campbell Scientific Ltd.). Raw data were sampled at a rate of 20 Hz and processed using the ECpack software to compute turbulent fluxes. The comparison between available energy ( $R_n - G$ ) and the sum of the sensible ( $H$ ) and latent (LE) heat fluxes shows a non-closure of the energy balance which is expected given the high complexity of the surface. The turbulent flux values used in this work were corrected using the approach proposed by (Twine et al. 2000) which is based on the hypothesis that the ratio  $H/LE$  is accurately measured than  $H$  and LE separately. Then, corrected turbulent fluxes were derived as  $LE = \frac{\beta}{\beta+1}(R_n - G)$  and  $H = \frac{(R_n - G)}{\beta+1}$ , with  $\beta$  computed from the 30-min observed  $H$  and LE. Additionally, a Large Aperture Scintillometer (LAS) was set up over a 1464 m transect spanning a representative area of the total site across the river between 10 and 50 m above the ground, with an effective height of  $\approx 26$  m. It consists of a transmitter installed at a height of 10.5 m and a receiver mounted at the height of 10 m (Fig. 1). Measurements were sampled at 1 Hz, averaged, and then stored at 30 min intervals on CR10X dataloggers. In this study, a footprint model proposed by Horst and Weil (1992, 1994) was applied to average the remote sensing data over the source areas where the turbulent fluxes were emanated (see Appendix 1).

## Remote sensing data

In this study, 17 satellite images were collected from Landsat 7 and 8. Combining the two satellites, a repeatability of eight days was reached. The resolution of the acquired images ranges from 30 to 100 m, depending on the spectral bands. The satellites products were downloaded from the USGS website (<https://earthexplorer.com/>). Nevertheless, the radiation measured by Landsat 7/8 has to be corrected from the atmosphere. To overcome this issue and derive actual land surface temperature (LST), the images were corrected following the steps described in Tardy et al. (2016). The corrections associated with the radiation emitted by the

atmosphere and to the atmospheric attenuation were based on the vertical atmospheric conditions (pressure, temperature, water vapor and ozone) of the ERA-Interim dataset. The atmospheric correction parameters were finally computed using the commercial RTM software MODTRAN. The surface emissivity was determined based on the vegetation index (NDVI) according to Wittich (1997).

## Evapotranspiration modelling

### Shuttleworth–Wallace model

Shuttleworth and Wallace developed a parameterization of the canopy evapotranspiration in 1985. This model considers two sources of water transfer from the surface to the atmosphere, from the soil by the evaporation process and from the vegetation through transpiration. For each source, the model takes into account both aerodynamic and surface resistances and assumes that the two sources will interact at the effective canopy's height considering another aerodynamic resistance between this height and the reference height source. The model is represented as follows:

$$ET = E + T = C_s PM_s + C_v PM_v \quad (1)$$

where  $E$  is the soil evaporation,  $T$  is the vegetation transpiration,  $PM_s$  and  $PM_v$  are terms similar to the Penman–Monteith combination equation.

They are expressed by the two following equations:

$$PM_s = \frac{\Delta A + [(\rho C_p D - \Delta r_a^s (A - A_s)) / (r_a + r_a^s)]}{\Delta + \gamma [1 + r_s^s / (r_a + r_a^s)]} \quad (2)$$

$$PM_v = \frac{\Delta A + [(\rho C_p D - \Delta r_a^v (A - A_s)) / (r_a + r_a^v)]}{\Delta + \gamma [1 + r_s^v / (r_a + r_a^v)]} \quad (3)$$

where  $A$  and  $A_s$  are the available energy above canopy and the soil surfaces ( $W/m^2$ ), respectively.  $\Delta$  is the slope of saturation vapour pressure curve (kPa/K),  $\rho$  is the air density ( $kg/m^3$ ),  $C_p$  is the specific heat of dry air at constant pressure ( $J/kg/K$ ),  $D$  is the water vapor deficit (kPa),  $\gamma$  is the psychrometric constant (Pa/K).

The coefficients  $C_s$  and  $C_v$  are given as follows:

$$C_s = \frac{1}{1 + [R_s R_a / R_v (R_s + R_a)]} \quad (4)$$

$$C_v = \frac{1}{1 + [R_v R_a / R_v (R_v + R_a)]} \quad (5)$$

where  $R_s$ ,  $R_v$ ,  $R_a$  are formulated as:

- 300  $R_s = (\Delta + \gamma)r_a^s + \gamma r_s^s$  (6) 343  
 301 344
- 302  $R_v = (\Delta + \gamma)r_a^v + \gamma r_s^v$  (7) 345  
 303 346
- 304  $R_a = (\Delta + \gamma)r_a$  (8) 347  
 305 348
- 306 where  $r_a^v$ ,  $r_a^s$ , and  $r_a$  are the aerodynamic resistance of the  
 307 canopy, the aerodynamic resistance between the reference  
 308 height and the effective height and from the effective height  
 309 to the soil surface (s/m), respectively. Additionally, soil  
 310 evaporation and plant transpiration are controlled by the  
 311 soil surface resistance ( $r_s^s$ ) and the canopy resistance ( $r_s^v$ ),  
 312 respectively. Both resistances are expressed as follow: 349
- 313  $r_s^s = r_{s\min}^s \left( 2.5 \left( \frac{\theta_F}{\theta_s} \right) - 1.5 \right)$  (9) 350  
 314 351
- 315  $r_s^v = \frac{r_{ST\min}}{\text{LAI} \prod_{i=1}^3 F_i(X_i)}$  (10) 352  
 316 353
- 317  $F_1(S) = \left( \frac{S}{1100} \right) \left( \frac{1100 + a_1}{S + a_1} \right)$  (11) 354  
 318 355
- 319  $F_2(T) = \frac{(T - T_L)(T_H - T)^{(T_H - a_2)/(a_2 - T_L)}}{(a_2 - T_L)(T_H - a_2)^{(T_H - a_2)/(a_2 - T_L)}}$  (12) 356  
 320 357
- 321  $F_3(\theta) = \begin{cases} 1, \theta \geq \theta_F \\ \frac{\theta - \theta_W}{\theta_F - \theta_W}, \theta_W < \theta < \theta_F \\ 0, \theta \leq \theta_W \end{cases}$  (13) 358  
 322 359
- 323 where  $r_{s\min}^s$  is the minimum soil surface resistance (taken as  
 324 100 s/m (Zhang et al. 2008)) and  $r_{ST\min}$  is the minimal stomatal  
 325 resistance of individual leaves under optimal conditions (taken  
 326 as 146 s/m (Zhang et al. 2008)).  $\theta_s$  is the water content of the  
 327 upper soil surface layer ( $\text{cm}^3/\text{cm}^3$ ). LAI is the leaf area index,  
 328 and  $F_i(X_i)$  is the stress function of the incoming photosyntheti-  
 329 cally active radiation flux (S), the air temperature (T) and the  
 330 actual soil moisture content in the root-zone ( $\theta$ ).  $T_H$  and  $T_L$   
 331 are the upper and lower temperature limits outside of which  
 332 transpiration is assumed to stop ( $^\circ\text{C}$ ) and are set at values of  
 333 40 and 0  $^\circ\text{C}$  (Harris et al. 2004).  $\theta_W$  is the soil moisture con-  
 334 tent at wilting point ( $\text{cm}^3/\text{cm}^3$ ),  $\theta_F$  is the soil water content at  
 335 field capacity ( $\text{cm}^3/\text{cm}^3$ ). The empirical coefficients  $a_1$  and  $a_2$   
 336 were derived by optimization and were set to 57.67 and 25.78  
 337 (Zhang et al. 2008), respectively.
- 338 The available energies above canopy and above the soil  
 339 surface are defined by the following expressions: where  $G$  is  
 340 the soil heat flux ( $\text{W}/\text{m}^2$ ) and  $R_n$  is the net radiation ( $\text{W}/\text{m}^2$ ).
- 341  $A = R_n - G$  (14) 389  
 342 390
- $A_s = R_n - G$  (15) 343  
 344
- $R_n$  is the net radiation fluxes into the soil surface ( $\text{W}/\text{m}^2$ )  
 which is parametrized as follows: where  $C$  is the extinction  
 coefficient of light attenuation, that equal to 0.68 for the fully  
 grown plant (Sene 1994). Moreover, resistance parameteriza-  
 tions are detailed in Zhang et al. (2008). 349
- $Rn_s = R_n e^{-C \times \text{LAI}}$  (16) 350  
 351
- Leaf area index (LAI) is derived from Landsat NDVI fol-  
 lowing Wang et al. (2008): 352  
 353
- $\text{LAI} = \begin{cases} 0, \text{NDVI} < 0.2 \\ \sqrt{\text{NDVI} \frac{1 + \text{NDVI}}{1 - \text{NDVI}}}, \text{NDVI} \geq 0.2 \end{cases}$  (17) 354  
 355
- Energy balance model and hourglass method** 356
- Soil energy balance model:* The soil energy balance model  
 was implemented to compute the endmembers temperature  
 ( $T_{s\min}$ ,  $T_{s\max}$ ,  $T_{v\min}$  and  $T_{v\max}$ ) further used in the Hourglass  
 method. The extremes soil temperature  $T_{s\min}$  and  $T_{s\max}$  were  
 simulated by forcing the surface resistances to 0 and  $\infty$ ,  
 respectively (Stefan et al. 2015; Merlin et al. 2016; Amazirh  
 et al. 2017, 2018). The model was initialized by the observed  
 air temperature and soil temperature is sought by minimiz-  
 ing the following cost function  $F$ : where  $H$  and  $LE$  are the  
 sensible and latent heat fluxes, respectively. 366
- $F = (R_n - G - H - LE)^2$  (18) 367  
 368
- The  $T_{v\min}$  was set to the air temperature measured over  
 the studied areas (Carlson et al. 1995; Bastiaanssen et al.  
 1998; Roerink et al. 2000; Merlin 2013; Stefan et al. 2015).  
 For  $T_{v\max}$ , it was defined according to the assumptions  
 described in Stefan et al. (2015), which considered the dif-  
 ferences between the extreme soil temperatures is the same  
 that between the extreme vegetation temperatures. 375
- Hourglass method:* Based on the strong relationship  
 between the variation of the cover fraction ( $fc$ ) and the sur-  
 face temperature (LST), Moran et al. (1994) determined a  
 polygon with four zones where each one is characterized  
 by a range of values of  $fc$  and LST. Merlin et al. (2012)  
 defined and separated four zones: transpiration- and evap-  
 oration-controlled, stressed and unstressed mixed surface.  
 The endmembers obtained with the soil energy balance were  
 used in the Hourglass method to determine the four zones.  
 Hereafter, the partitioning of LST into its soil and vegetation  
 components is based on the LST and  $fc$  within the polygon  
 to determine one of the temperature components  $T_v$  or  $T_s$   
 (see Appendix 2). 388
- Soil and vegetation temperature estimations:* A time series  
 of vegetation and soil temperatures ( $T_v$  and  $T_s$ ) and their 390

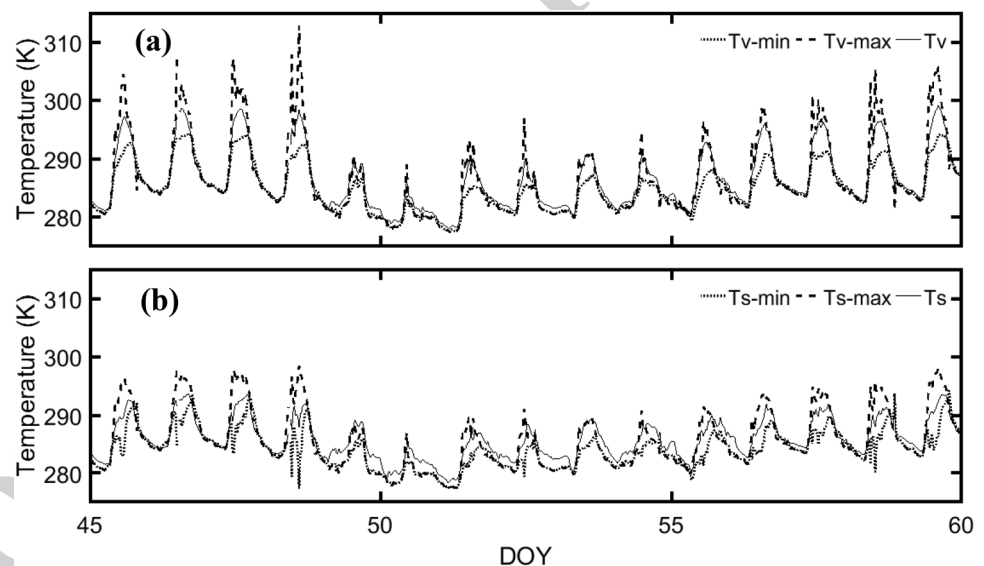
391 corresponding endmembers ( $T_{s_{\min}}$ ,  $T_{s_{\max}}$ ,  $T_{v_{\min}}$  and  $T_{v_{\max}}$ )  
 392 from day of the year 45–60 (2017) are shown in Fig. 2. In this  
 393 section, LST used in Eq. 32 was inverted from the longwave  
 394 radiation emitted by the surface and measured using CNR4  
 395 as follow:

$$396 \text{ LST} = \left( \frac{\text{LW}}{\varepsilon \sigma} \right)^{1/4} \quad (19)$$

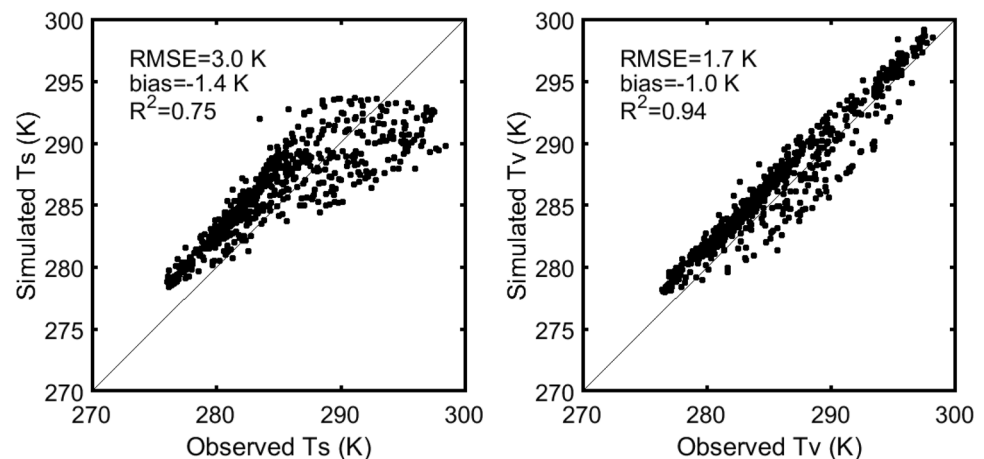
397 where LW is the longwave radiation emitted by the surface,  
 398  $\varepsilon$  is the surface emissivity and  $\sigma$  is the Stefan-Boltzmann  
 399 constant. This period was chosen to illustrate the variation  
 400 of the different temperatures since it coincides with the  
 401 development stage of the wheat that presents a mixture of  
 402 soil and vegetation. The two temperatures  $T_v$  and  $T_s$  ranged  
 403 between their minimum and maximum values supporting  
 404 the good performances of the Hourglass method. To vali-  
 405 date the two components  $T_v$  and  $T_s$  of the partition of the  
 406

LST, both were compared against soil and vegetation tem-  
 407 perature observations (Fig. 3).  $T_v$  is well reproduced with  
 408 an RMSE and  $R^2$  equal to 1.6 K and 0.94, respectively. By  
 409 contrast, the simulated  $T_s$  is not as good with an RMSE and  
 410  $R^2$  of about 3 K and 0.76, respectively. It is clearly seen that  
 411 both temperatures  $T_s$  and  $T_v$  are overestimated, with a bias  
 412 equal to  $-1.4$  K and  $-1$  K for  $T_s$  and  $T_v$ , respectively. This  
 413 scattering can be justified by numerous factors. As  $T_v$  was  
 414 computed first for most of the time while  $T_s$  was deducted  
 415 from Eq. 32. Meaning that  $T_s$  accumulated errors of both  $T_v$   
 416 and LST. Likewise, the discrepancy can be related to the  
 417 estimation of  $f_c$  from Landsat NDVI, as the Landsat pixel  
 418 size is larger than the surface of view of the IRT-Apogee.  
 419 This will obviously lead to some errors in the partition of  
 420 temperature between soil and vegetation. Another reason  
 421 that can probably explain the discrepancy is the location  
 422 of the measurements. As reported by Olivera-Guerra et al.  
 423 (2018) the youngest leaves of the plant are expected to be  
 424

**Fig. 2** Variation of soil (a) and vegetation (b) temperatures derived from Hourglass method, and their maximum and minimum computed from soil surface energy balance model, from DOY 45 to DOY 60



**Fig. 3** Simulated soil and vegetation temperatures versus in situ measurements for the same period as Fig. 2



425 colder than the adult and senescing leaves, whose tempera- 454  
 426 ture has not been measured. Otherwise, by comparing both 455  
 427 simulated  $T_s$  and  $T_v$  temperatures in terms of magnitude it 456  
 428 can notice that  $T_v$  is superior to  $T_s$ .  $T_s$  never exceeds 294 K 457  
 429 although  $T_v$  reaches 300 K. This can be explained by the 458  
 430 plotting period of  $T_s$  and  $T_v$  that coincides with the develop- 459  
 431 ment stage of wheat planted under olive trees and thus there 460  
 432 was no bare soil surface. As well as,  $T_s$  can be lower than 461  
 433  $T_v$  during rainfall or irrigation events. Overall, these results 462  
 434 are in agreement with the values reported in the literature 463  
 435 (Stefan et al. 2015; Olivera-Guerra et al. 2018). Soil and 464  
 436 vegetation temperatures and their endmembers are used to 465  
 437 calculate the two stress indexes related to the soil ( $SI_{ss}$ ) and 466  
 438 to the vegetation ( $SI_{sv}$ ), and finally to estimate spatial ET by 467  
 439 the SW model.

440 **Spatialization of the SW model**

441 ET derived by the SW model showed a good consistency at 470  
 442 the local scale (Zhang et al. 2008; Zhu et al. 2013, 2014). 471  
 443 However, to our knowledge, no study tried to spatialize the 472  
 444 SW model since many variables are required especially, for 473  
 445 the soil and the vegetation resistances ( $r_s^s$  and  $r_s^v$ ) computa- 474  
 446 tion. As mentioned above, this work aims to retrieve the 475  
 447 resistances using accurate values of transpiration and evapo- 476  
 448 ration and to suggest a relationship between the retrieved 477  
 449 resistances and the stress indexes based on the measured 478  
 450 LST. In fact, retrieving these resistances from measure- 479  
 451 ments based on the equations of the SW model is very 480  
 452 difficult mathematically. To overcome this issue, the Shut- 481  
 453 tleworth–Wallace model has been used to retrieve the two

resistances values based on a very small threshold conver- 454  
 455 gence (less than  $2 \text{ W/m}^2$ ) defined as the absolute value of the 456  
 457 difference between simulated ( $ET_{SW}$ ) and measured ( $ET_{EC}$ ) 458  
 459 evapotranspiration. This threshold is chosen based on the 460  
 461 reliability of the simulated values and on their number to get 462  
 463 enough points to develop the relationship between the indi- 464  
 465 ces and the resistances. Hereafter, an empirical exponential 466  
 467 relationship was developed between the retrieved resistances 468  
 469 and the soil and the vegetation stress indexes ( $SI_{ss}$ ,  $SI_{sv}$ ). 470  
 471 These latter were computed using the endmember tempera- 472  
 473 tures deduced from the soil energy balance model and the 474  
 475 vegetation and the soil temperature calculated using Hour- 476  
 477 glass method as follow:

$$SI_{ss} = \frac{T_s - T_{s_{min}}}{T_{s_{max}} - T_{s_{min}}} \quad (20)$$

$$SI_{sv} = \frac{T_v - T_{v_{min}}}{T_{v_{max}} - T_{v_{min}}} \quad (21)$$

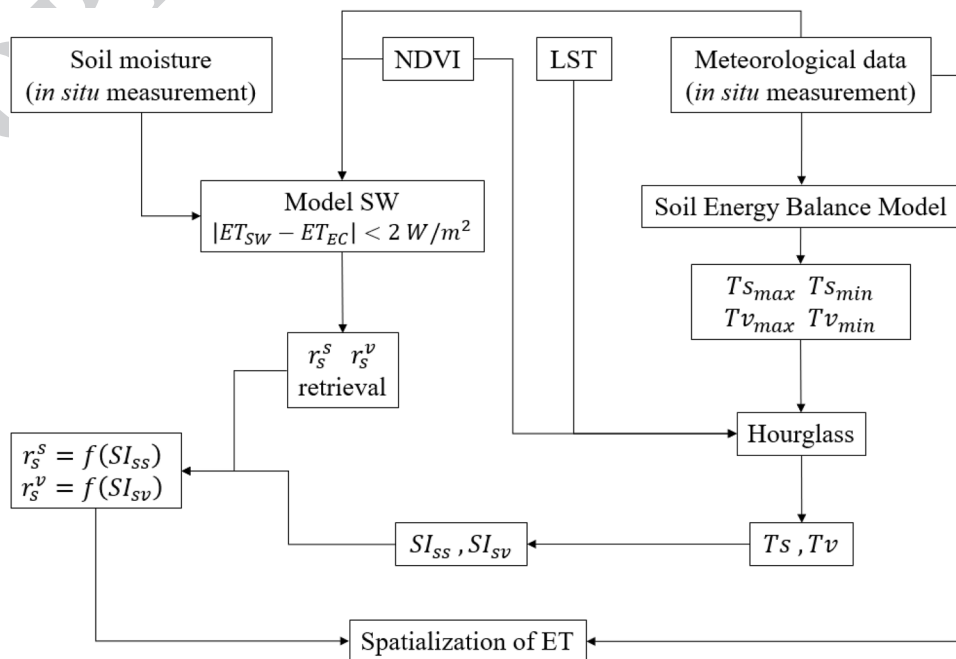
An overview of the methodology is summarized in Fig. 4.

**Results**

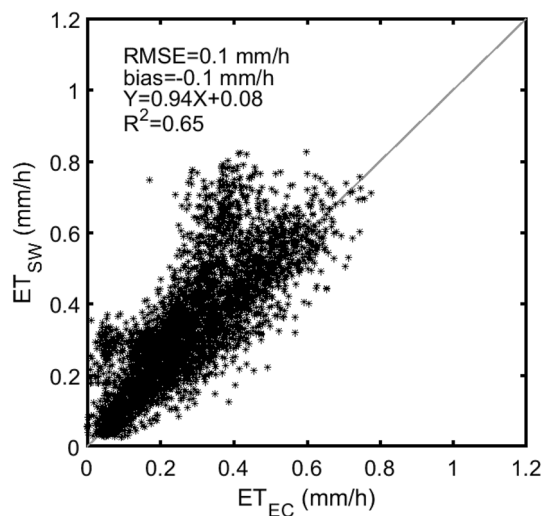
**In situ evaluation of the SW model**

Figure 5 presents a comparison between the half-hourly ET 474  
 475 measured by eddy covariance system (average of 0.26 mm/h) 476  
 477 and simulated (average of 0.30 mm/h) by the original SW 478  
 479 model based on the soil moisture data to compute soil and 480  
 481

Fig. 4 Flowchart of the proposed approach







**Fig. 5** Half-hourly comparison between evapotranspiration predicted by the Shuttleworth–Wallace model ( $ET_{SW}$ ) and measured by the Eddy covariance system ( $ET_{EC}$ ) during 2017

478 vegetation resistances, during the 2017 growing season. This  
 479 figure shows that the linear regression between simulated  
 480 and in situ ET is very encouraging with a slope and an intercept  
 481 of about 0.94 and 0.08 mm/h, respectively. According  
 482 to the statistical analysis depicted in this figure, the model  
 483 simulations are acceptable with a relative RMSE, bias and  
 484  $R^2$  of about 0.38,  $-0.1$  mm/h and 0.65, respectively. The  
 485 obtained results indicate that the model is able to predict  
 486 ET over surface with a high degree of canopy cover hetero-  
 487 geneity. The scatter of modeled ET is mainly due to canopy  
 488 uniformity over the surface. Moreover, the experimental plot  
 489 is irrigated differently during the season. In fact, the farmer  
 490 irrigates the entire surface when the wheat was cultivated  
 491 under the olive trees. By contrast, when there is no wheat,  
 492 the irrigations were limited to the tree rows. This can create  
 493 a large heterogeneity over the EC footprint. Additionally,  
 494 this heterogeneity can affect the soil and vegetation resist-  
 495 ances which were estimated using data acquired near the EC  
 496 tower. Another major issue that can explain the differences  
 497 between measured and simulated ET is the non-closure of  
 498 the energy balance at the EC system level. The compar-  
 499 ison between the available energy and the turbulent fluxes  
 500 shows that the sum of the turbulent fluxes only reaches 60%  
 501 of the available energy. This non-closure is similar to what  
 502 has been observed in previous studies (Mauder et al. 2006;  
 503 Liu et al. 2011) and can be considered acceptable due to  
 504 the complexity of the study site. In fact, the EC measure-  
 505 ments were corrected using Bowen ratio method (Twine  
 506 et al. 2000). However, the correction was not ideal due to  
 507 the storage and the photosynthesis terms which were not  
 508 taken into consideration. Additionally, the footprint devices  
 509 of the EC system, the CNR4 radiometer and the soil flux

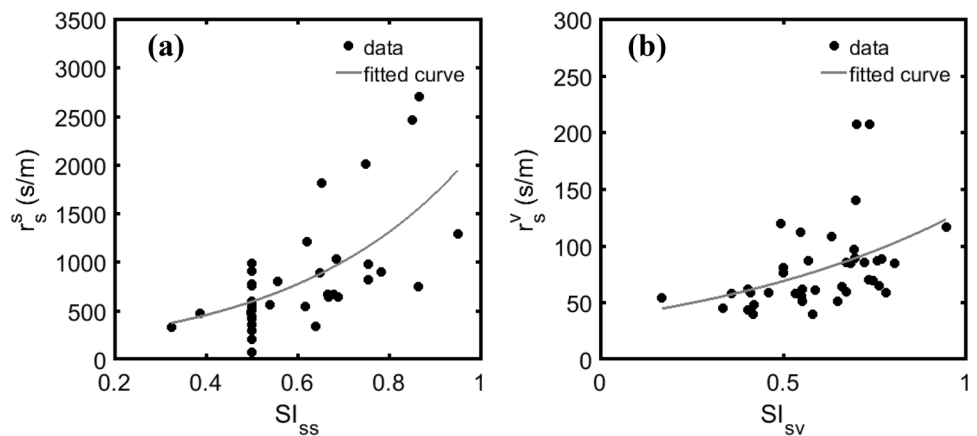
510 plaques were quite different. Furthermore, the soil heat flux  
 511 was measured using a heat flux plate, which does not take  
 512 into consideration the heat storage in the soil layer above  
 513 it. This error related to the G measurements can affect the  
 514 Bowen correction of the EC measurements and consequently  
 515 the comparison between simulated and measured ET.

516 As reported by Zhang et al. (2009), when the soil was  
 517 partially wetted the SW model tends to overestimate ET  
 518 by 25.2% over a vineyard. Likewise, Zhang et al. (2008)  
 519 found that this model overestimates the ET over a vineyard  
 520 in an arid desert region with a mean absolute error (MAE)  
 521 of about 0.057 mm/h. On the contrary, some studies showed  
 522 that the SW model underestimated half-hourly ET. Zhu et al.  
 523 (2014) indicated that the SW model tended to underestimate  
 524 the half-hourly ET with a RMSE value of 0.12 mm/h and a  
 525 maximum nearly equal to 0.88 mm/h over the spring maize  
 526 in the arid desert oasis. Also, Ortega-Farias et al. (2010)  
 527 reported that the SW model underestimated on half-hourly  
 528 time intervals compared to the EC-measured ET over a  
 529 drip-irrigated Merlot vineyard in a Mediterranean semi-  
 530 arid region during the growing season in 2006/2007 with a  
 531 RMSE equal to 0.046 mm/h and a maximum nearly equal  
 532 to 0.59 mm/h. Therefore, the performance of the SW model  
 533 seemed to be variable for different crops and places. Further-  
 534 more, several parameters used in the model are set to con-  
 535 stant values throughout the study period without considering  
 536 the seasonal changes. This may impact the quality of the ET  
 537 predictions, in particular for the physiology-related param-  
 538 eters. In addition, Hu et al. (2009) and Zhu et al. (2013)  
 539 reported that for long-term simulations of ET, a systematic  
 540 overestimation or underestimation may occur when constant  
 541 parameters are used during different vegetation and environ-  
 542 mental conditions. The simulated values chosen to retrieve  
 543 the soil and vegetation resistances were selected based on  
 544 the good simulation of ET by the SW model when the gap  
 545 between simulated and measured ET is less than  $2 \text{ W/m}^2$ .

### 546 Local evaluation of the proposed approach

547 Figure 6 displays the relationship between the retrieved  
 548 resistances ( $r_s^s$  and  $r_s^v$ ) and the stress indexes ( $SI_{ss}$  and  $SI_{sv}$ ),  
 549 respectively. The values have been chosen between 12 and  
 550 15 h which correspond to the maximum of radiation. The  
 551 resistance variation ranges (0–3000 s/m for  $r_s^s$  and 0–250 s/m  
 552 for  $r_s^v$ ) presented in Fig. 6 are in good agreement with those  
 553 obtained in the literature (Ortega-Farias et al. 2010; Zhu  
 554 et al. 2014; Zhao et al. 2015). In addition, the obtained trend  
 555 is similar to that found by Ortega-Farias et al. (2010), Bren-  
 556 ner and Incoll (1997) and Zhao et al. (2015) between the  
 557 soil resistance and the soil humidity which is replaced in  
 558 this work by the stress indexes. Note, that the stress indexes  
 559 represent dry conditions when they tend towards 1 and wet  
 560 conditions when they are close to 0. Figure 6a presents some

**Fig. 6** Relationships between the soil (a) and vegetation (b) resistances ( $r_s^s$  and  $r_s^v$ ) and two stress indexes ( $SI_{ss}$ ,  $SI_{sv}$ ) derived from Eqs. 22, 23 for the values between 12 and 15 h. The best fit was also presented (solid line)



561 soil resistance corresponding to the same stress index value  
 562 ( $SI_{ss} = 0.5$ ). These (LST,  $f_c$ ) points were situated in the  
 563 transpiration-control zone (see Appendix 2). In this zone  $T_s$   
 564 was calculated as the average of their endmembers (Eq. 27).  
 565 The stress index was calculated as the ratio of the differ-  
 566 ence between  $T_s$  and  $T_{s_{min}}$  and the difference between  $T_{s_{max}}$   
 567 and  $T_{s_{min}}$ . Consequently, the stress index will be continu-  
 568 ally equal to 0.5 in this zone. This problem was not seen  
 569 in Fig. 6b for the vegetation resistance since there are few  
 570 (LST,  $f_c$ ) points located in the evaporative control zone. The  
 571 figure shows the best fits obtained between the soil and the  
 572 canopy resistances and the stress indexes which are given by:

$$573 \quad r_s^s = ae^{b \times SI_{ss}}, \quad R = 0,6 \quad (22)$$

574

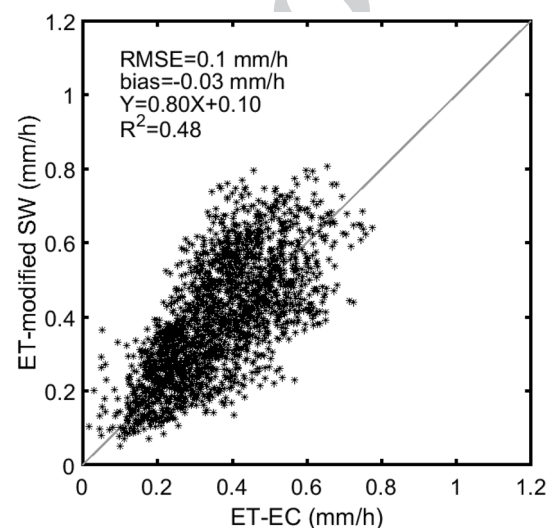
$$575 \quad r_s^v = ce^{(d \times SI_{sv})}, \quad R = 0,5 \quad (23)$$

576

577

578 Where the calibration parameters a, c, b and d are equal  
 579 to 160.25 and 36.02 s/m, 2.62 and 1.30, respectively. Note  
 580 that the values of these parameters are expected to depend  
 581 on the canopy, on the local meteorological conditions and  
 582 on the soil types. Exponential fitting was chosen after test-  
 583 ing numerous fitting types given its good representativity of  
 584 the points scatter.

585 For the validation of the proposed approach based on  
 586 optical (NDVI) and thermal (LST) data to compute soil and  
 587 vegetation resistances in SW model, a comparison between  
 588 the predicted (average of 0.37 mm/h) and measured (average  
 589 of 0.34 mm/h) ET at the station scale was illustrated in  
 590 Fig. 7. The obtained linear regression between simulated  
 591 and in situ ET is very encouraging with a slope and an inter-  
 592 cept of about 0.8 and 0.1 mm/h, respectively. The results  
 593 are acceptable with a relative RMSE, bias and a  $R^2$  of about  
 594 0.29,  $-0.03$  mm/h and 0.48, respectively. The discrepan-  
 595 cies in the estimation of ET can be related to the error in  
 596 the LST estimations and in its partitioning. The statistical  
 597 performances obtained were in concordance with other



**Fig. 7** Half-hourly comparison between estimated ET using the proposed approach and measured one by the Eddy covariance system from January to June 2017

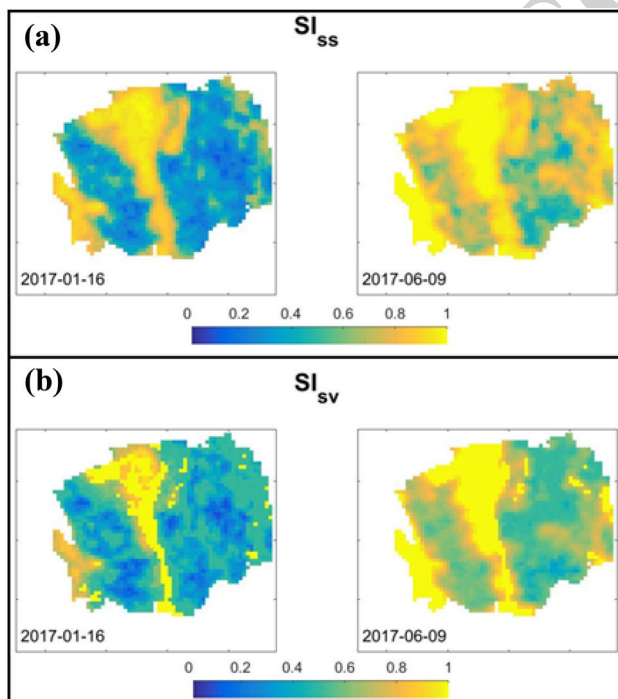
588 studies that used the thermal proxy based on LST such as (i) 598  
 599 FAO-2Kc model used by Olivera-Guerra et al. (2018), who 599  
 600 found a RMSE of 0.08 mm/h and  $R^2$  of 0.75 over a wheat 600  
 601 plot using daily average values, (ii) Penman–Monteith equation 601  
 602 used by Amzirh et al. (2017) who found a RMSE of 602  
 603 about 0.12 mm/h and a  $R^2$  of 0.53 over a wheat plot, and (iii) 603  
 604 TSEB model where Diarra et al. (2017) obtained a RMSE 604  
 605 of 0.10 mm/h and a  $R^2$  of 0.67 over a sugar beet field and a 605  
 606 RMSE of 0.11 mm/h and  $R^2$  of 0.42 over a wheat field. 606

## 607 Spatial evaluation of the proposed approach

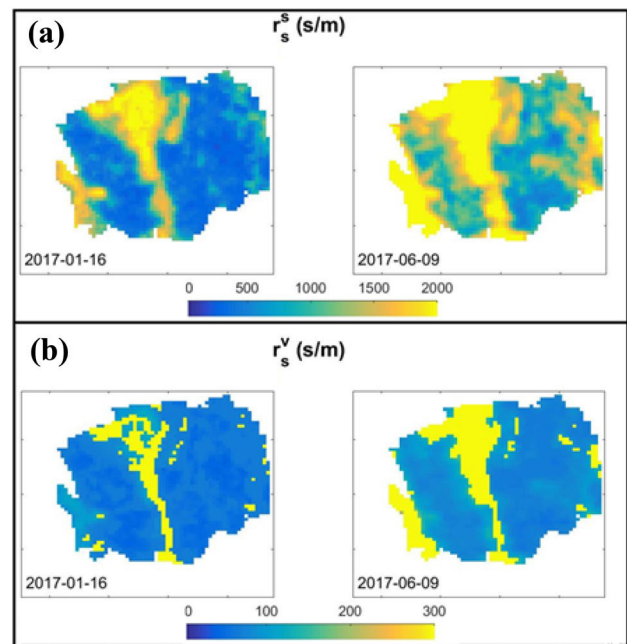
### 608 Stress indexes and resistances spatialization

609 The SW model has been used to spatialize the evapotranspi- 609  
 610 ration over the piedmont zone. The inputs used in the calcu- 610  
 611 lation of the soil and vegetation resistances are difficult to be 611

612 spatialized given the need for soil moisture (SM) maps with  
 613 high spatial resolution. Indeed, global soil moisture prod-  
 614 ucts are generally derived from passive microwave radiom-  
 615 eters with a spatial resolution exceeding 10 km, largely too  
 616 coarse for hydrological applications or from the active one  
 617 which can provide soil moisture products with high spatial  
 618 resolution but using complexed method. By contrast, opti-  
 619 cal and thermal remote sensing data are available with high  
 620 spatial resolution. Consequently, to overcome this issue the  
 621 Landsat data have been used instead of the SM to calculate  
 622 the soil and vegetation resistances using the new proposed  
 623 approach. Figure 8 presents the spatial variation of the two  
 624 stress indexes ( $SI_{ss}$  and  $SI_{sv}$ ) at two dates in winter (2017-01-16)  
 625 and summer (2017-06-09) periods. The stress indexes  
 626 range between 0 (no stress) and 1 (severe stress) depend-  
 627 ing on the hydric state of the surface. For both dates, the two  
 628 indexes exhibited as expected values close to 1 at the river  
 629 level since there were no growing plants. By contrast, the  
 630 areas covered by vegetation are characterized by values of  
 631  $SI$  lower than 1. Both stress indexes achieved high values  
 632 in summer (date 2017-06-09) exceeding 0.6 which can be  
 633 justified by the absence of water supply. This is compat-  
 634 ible with the available water since the irrigation system is  
 635 based on surface water that occurs as a result of melting  
 636 snow. Figure 9 represents the corresponding soil and vegeta-  
 637 tion resistances, computed from two stress indexes through



**Fig. 8** Maps of the soil ( $SI_{ss}$ ) and vegetation ( $SI_{sv}$ ) stress index over the study area for two contrasted dates (2017-01-16) and (2017-06-09)



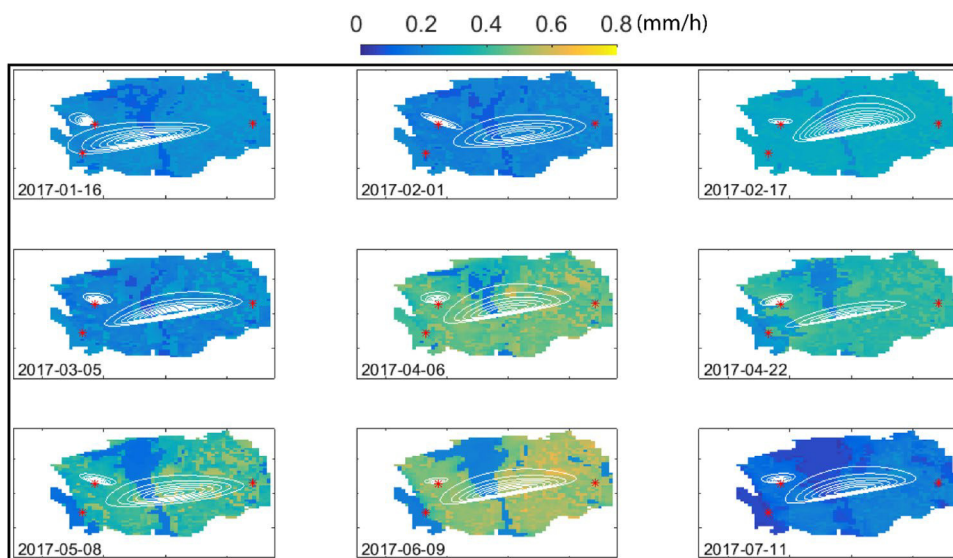
**Fig. 9** Maps of the soil ( $r_s^s$ ) and vegetation ( $r_s^v$ ) resistance over the study area for two dates (2017-01-16) and (2017-06-09)

two relationships proposed above (Eqs. 22, 23). Vegetation resistance is obviously very high along the river bed since the LAI tends to zero and leads to negligible transpiration. Soil resistance reflects the temporal and spatial variation of the surface soil moisture on the study area. High soil resistance values lead to a sharp decrease in evaporation which is produced by the increase in solar radiation reaching the surface and the low irrigation supply.

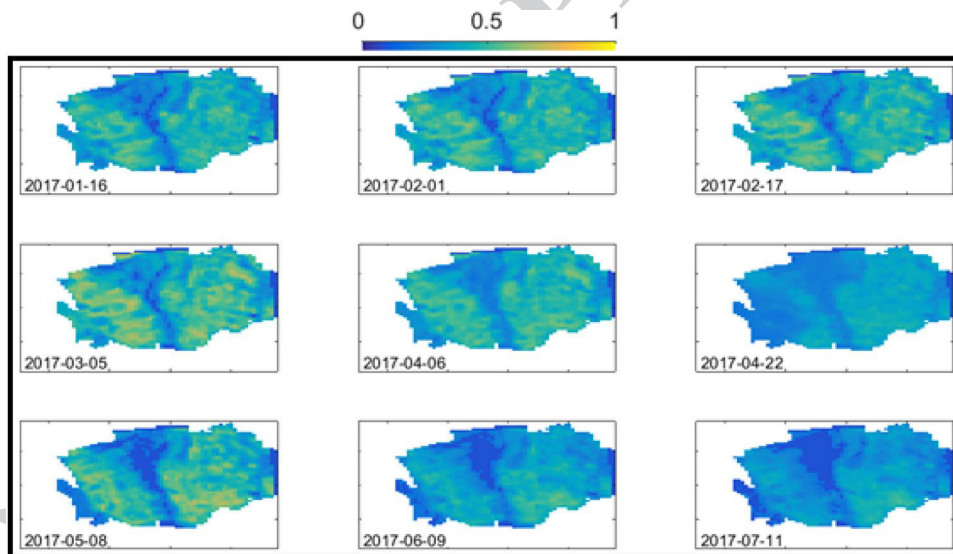
### Evapotranspiration mapping

Figure 10 displays the spatial and temporal distributions of ET from winter to summer of 2017. For that, 17 Landsat images have been used but only 9 images acquired by Landsat-7 are plotted for illustrating purpose. The spatial distribution of ET is tightly linked to the spatial variation of the fraction cover (Fig. 11), with low values along the river bed which represents a bare soil surface and higher overall the study site which contains a diversity of croplands and arboriculture especially olive trees. The use of an averaged  $fc$  value integrating different heterogeneous crops which are located within one Landsat pixel can generate some uncertainties in the ET estimates. Indeed, the transpiration for each type of crops is different and depends on its response to the stress conditions due to the difference of LAI and rooting depth. In practice, values of LAI should be calculated for each crop within one Landsat pixel and afterwards a specific formula should be used for deriving the correspondent  $fc$  of each LAI value. However, this solution cannot be applied in

**Fig. 10** Evapotranspiration (mm/h) maps over the study area for the dates of the Landsat-7 overpass. The footprint of LAS and EC for the time of the satellite overpass is also represented



**Fig. 11** Fraction cover maps over the study area for the dates that coincide with the overpass of Landsat-7

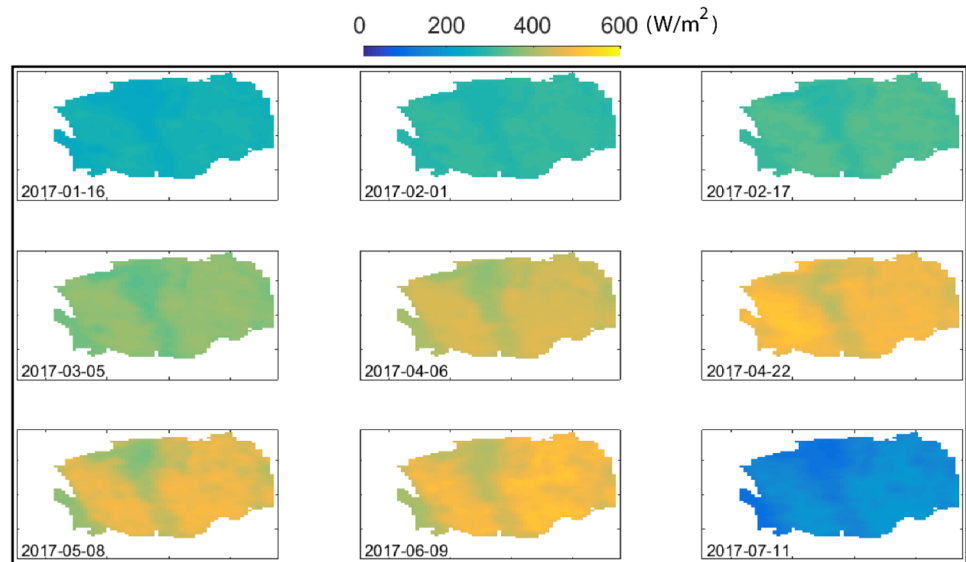


665 this study due to the complexity of the site. Therefore, it can  
 666 be concluded that although great progress has been made  
 667 in the development of the satellites particularly in terms of  
 668 spatial resolution, the heterogeneity of our site is one of the  
 669 major challenges that must be overcome to use the satellite  
 670 data to assess evapotranspiration in that orchards. Another  
 671 issue that can generate some uncertainties in the ET estimates  
 672 over our site was the difficulties of measuring  $T_v$ . In  
 673 fact, measured  $T_v$  used in this study was a value attributed  
 674 to the whole vegetation which means that the same resistance  
 675 value was attributed to the different crops. In practice,  
 676 it is difficult to have an adequate place to install the Infra-  
 677 Red radiometer sensor for providing measurements that can  
 678 be representative of the whole vegetation in such complex  
 679 area. To avoid this problem, we need to install an Infra-Red

radiometer over each crop which is not feasible as explained  
 for  $f_c$  issue. Otherwise, the estimated  $T_v$  using the energy  
 balance model and the hourglass method represents the whole  
 vegetation, meaning that no separation between crops was  
 considered. Consequently, to improve the transpiration  
 estimates using the proposed model, as mentioned before,  
 a high spatial resolution of satellite data is required over  
 such complexity to distinguish between different types of  
 crops. Figure 10 shows also a significant seasonal variation  
 of ET values ranging from less than 200 to up to 520  
 $W/m^2$ . This variation is mainly related to the available  
 energy and the fraction cover which increase progressively  
 in time from winter to early summer when wheat is  
 harvested (Figs. 11, 12). However, in the fifth day of  
 March, ET values were low even while the available energy  
 was significant (an average

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**Fig. 12** Available energy ( $\text{W}/\text{m}^2$ ) maps over the study area for the dates that coincide with the overpass of Landsat-7

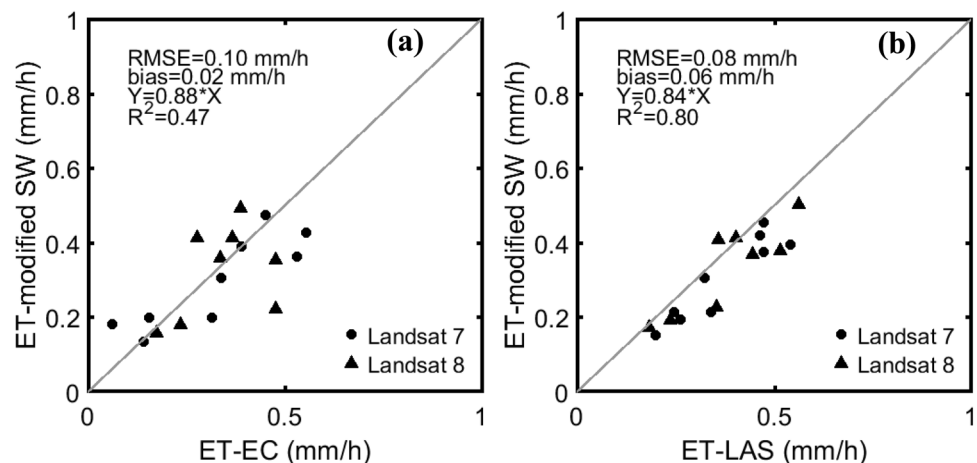


695 of about  $420 \text{ W}/\text{m}^2$ ) and the fraction cover was high (an  
696 average of about 0.65). This is attributed to the atmospheric  
697 saturation, as the air temperature was low (about  $14 \text{ }^\circ\text{C}$ )  
698 and the air humidity was high (71.45%). This drastically  
699 decreased the amount of the evaporative demand.

700 The footprints of the scintillometer and EC were also  
701 presented in Fig. 10 to show the variation of the source area  
702 of the LAS and EC measurements. The footprint was used  
703 to weight the ET values from the maps at the time of the  
704 satellites overpass. The modeled ET values were validated  
705 by comparing them to the measurements (over the LAS and  
706 EC footprints). Figure 13 shows good consistency between  
707 the simulated ET values, using SW model driven by Landsat  
708 7 and 8 and observed one. The statistical analysis between  
709 the model and the LAS measurements showed better agree-  
710 ment than those obtained between the model and the EC  
711 measurements with an RMSE and  $R^2$  of about 0.08 mm/h  
712 and 0.80, respectively, for the LAS and 0.1 mm/h and 0.47,

713 respectively, for the EC. This can be justified by the accu-  
714 racy of the relation between the resistances and the stress  
715 indexes which could be stronger over other plots than the  
716 plot where the calibration was done. Otherwise, the com-  
717 parison with EC and LAS measurements show an underesti-  
718 mation with a slope of about 0.84 and 0.88 for LAS and EC,  
719 respectively. This underestimation of the ET by the model  
720 is probably justified by the error on the satellites LST. The  
721 processing of this data as mentioned in Sect. (Remote sens-  
722 ing data) can cause a surface temperature overestimation.  
723 This will generate an overestimation of the resistances and  
724 consequently, the ET will be underestimated. Additionally,  
725 in our model, for an NDVI less than 0.2 the LAI is set to  
726 0 while, some sparse vegetation can grow along the river  
727 which is not enough to exceed the NDVI threshold. This  
728 can provide low estimated ET. The results obtained are rel-  
729 evant compared to other studies that used the scintillometry  
730 method to evaluate the performance of the different model

**Fig. 13** Comparison of esti-  
mated evapotranspiration from  
the modified SW model driven  
by Landsat-7 and Landsat-8  
and measured by the eddy  
covariance system (a) and the  
scintillometer (b)



731 in estimating ET. Ait Hssaine et al. (2018) have found an  
 732 RMSE and  $R^2$  of about 0.11 mm/h and 0.52, respectively,  
 733 between scintillometer measurement and ET estimated using  
 734 the Two-source Energy Balance model (TSEB) over an het-  
 735 erogeneous area covered by Millet (58%), Fallow savannah  
 736 (23%) and Degraded shrubs (19%) in the region of Niamey  
 737 city, Niger. In the same vein, Saadi et al. (2018) have used  
 738 an extra-large scintillometer to validate ET values estimated  
 739 using Soil Plant Atmosphere and Remote Sensing Evapo-  
 740 transpiration (SPARSE) model over a landscape dominated  
 741 by agriculture products (cereals, olive groves, fruit trees,  
 742 market gardening). They found a RMSE and  $R^2$  of about  
 743 0.06 mm/h and 0.55, respectively.

744 The proposed approach has some limitations compared  
 745 to traditional models such as SEBAL or METRIC. In fact,  
 746 these models don't need an accurate surface temperature  
 747 which demands complicated treatments and corrections  
 748 (Allen et al. 2007; Gonzalez-Dugo et al. 2009) or air tem-  
 749 perature measurements. In contrary, our approach requires  
 750 accurate values of surface temperature to correctly esti-  
 751 mate the different resistances. Otherwise, Choi et al. (2009)  
 752 reported that METRIC forces the predicted flux distributions  
 753 to scale between wet and dry hydrologic conditions, which  
 754 may not necessarily be present in every image. In contrast,  
 755 the proposed approach does not make this assumption and  
 756 depend only on moisture variability represented by the stress  
 757 indexes in the model. In addition, the proposed approach  
 758 is a two-source model which allows to the ET partitioning  
 759 into soil evaporation (E) and plant transpiration (T). This is  
 760 an important advantage that provides precise information  
 761 about the real amount of water needs by crops. However, in  
 762 this study, the partition of the soil evaporation and the tran-  
 763 spiration was not evaluated given the unavailability of the  
 764 measurement devices of separate E/T in the study area. The  
 765 proposed approach was calibrated over olive tree with an  
 766 understory of annual crops. The established relation between  
 767 the stress indexes and the resistances (Eqs. 22, 23) over this  
 768 type of cover may need to be adapted over other vegetation  
 769 types which their sensitivity to the stress conditions is differ-  
 770 ent. Otherwise, although the study site presents a high het-  
 771 erogeneity of vegetation type, the proposed approach shows  
 772 good consistency when the simulation values were compared  
 773 to the LAS measurements. Overall, this modification of the  
 774 SW model is needed to be tested with other data set and over  
 775 other meteorological conditions to evaluate its robustness  
 776 and improve the relation found between the resistances and  
 777 the thermal stress indexes.

778 The proposed approach has a great potential for esti-  
 779 mating ET over complex surface. This provides a precise  
 780 information about the real amount of crops water needs  
 781 for improving large scale sustainable irrigation strategy. In  
 782 addition, the use of thermal/optical remote sensing data has  
 783 proven to be remarkably accurate and robust for estimating

the ET over complex and heterogeneous area. However, test-  
 ing this approach with other data set and over other meteoro-  
 logical conditions to evaluate its robustness and improve the  
 relation found between the resistances and the thermal stress  
 indexes is necessary. Likewise applying other constraint on  
 soil evaporation and plant transpiration as the soil moisture  
 derived from the microwave data will be of great importance  
 to improve the soil and vegetation resistances estimates.

## Conclusion

Accurate and consistent estimation of evapotranspiration is  
 essential in determining the crop water requirement. The aim  
 of this work was to map the ET over a heterogeneous surface  
 in the piedmont of Atlas mountain using the SW model.

The spatialization of this model requires knowledge of the  
 spatial variation of certain inputs such as the soil moisture  
 which is not easy to be obtained with high spatial resolution  
 taking into account the heterogeneity of the site. The idea  
 that has been proposed is to use the thermal and optical  
 data provided from Landsat 7 and 8 instead to soil moisture  
 which is difficult to obtain. Soil and vegetation resistances  
 $(r_s^s, r_s^v)$  were linked to the stress indexes which are computed  
 from a normalization of vegetation and soil temperature by  
 their endmembers. The vegetation and soil temperatures are  
 derived using the Hourglass method forced by vegetation  
 fraction and meteorological data. The endmembers of the  
 two surface temperature components are simulated using a  
 surface energy balance model. The following conclusions  
 were drawn from the results of the study:

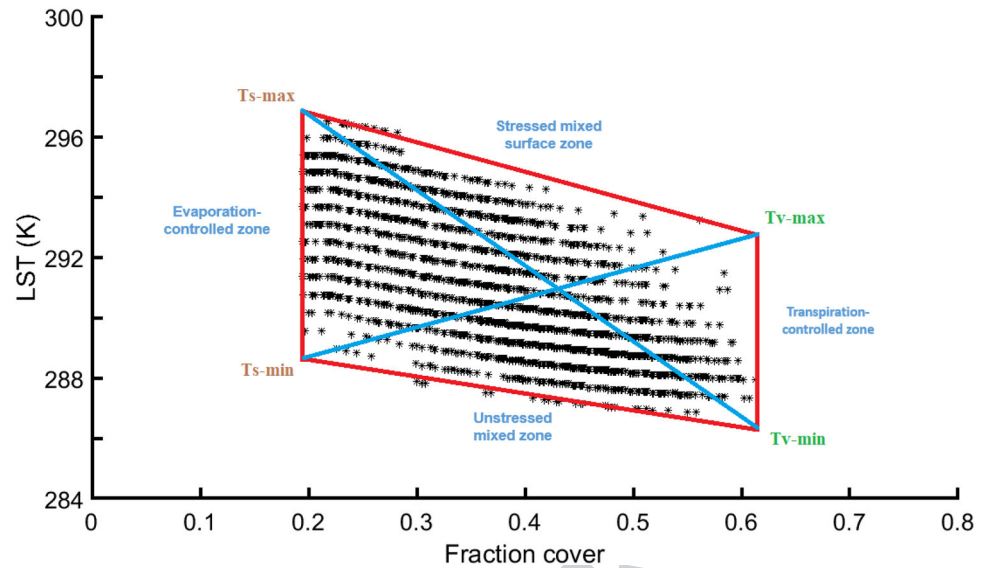
First, SW model was tested locally and acceptable results  
 were obtained in estimating ET with a relative RMSE and  
 bias are equal to 0.38 and  $-0.1$  mm/h, respectively.

Second, the resistances values were inverted from the SW  
 model and used to found the empirical relations based on  
 the stress indexes. The method was validated at local scale  
 by comparing the results with EC system and the statistical  
 performance were encouraging with a relative RMSE and  
 bias equal to 0.29 and  $-0.03$  mm/h, respectively.

Finally, the proposed approach was spatialized using  
 Landsat 7 and 8 data and confirmed its accuracy by compari-  
 son to the LAS and EC measurements. The RMSE, bias and  
 $R^2$  are equal to 0.08 mm/h, 0.06 mm/h and 0.80, respectively,  
 compared to the LAS and equal to 0.1 mm/h, 0.02 mm/h and  
 0.47, respectively, compared to the EC.

This approach proves the utility of thermal and optical  
 remote sensing for estimating accurate ET at a regional  
 scale. This will be even better if these data were provided  
 with a high revisit time keeping the same spatial resolu-  
 tion. Such improvement is possible with the advent of the  
 TRISHNA mission as reported by Lagouarde and Bhat-  
 tacharya (2018). In addition to optical and thermal data

**Fig. 14** Illustration of a polygon defined in the land surface temperature-fractional vegetation cover space contains four distinct zones (Evaporation-controlled zone, stressed mixed surface zone, transpiration-controlled zone and unstressed mixed zone)



834 other relevant remote sensing product could be used to  
835 feed the proposed approach. In particular, the microwave  
836 data, which are strongly related to the soil hydric status,  
837 can provide a promising issue to improve irrigation man-  
838 agement. Finally, it should be noted that the procedure  
839 proposed here has been solely tested during one growing  
840 season. Further tests of this procedure with other data sets  
841 and over other surface conditions are needed.

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## 850 Appendix 1

851 The LAS measurement is the average of an entire area  
852 where each part of it contributes with a percentage  
853 depends on its position, weight and wind speed. To obtain  
854 this contribution several analytical and Lagrangian models  
855 of footprint have been developed (Schuepp et al. 1990;  
856 Horst and Weil 1992; Rannik et al. 2000). In this work,  
857 we used the model of Horst and Weil (1992) that relates  
858 the flux measured at  $z_m$  to the surface distribution of the  
859 flux: where  $f$  is the footprint function relates the flux meas-  
860 ured at  $z_m$ ,  $F(x, y, z_m)$  to the spatial distribution of surface  
861 fluxes,  $F(x, y, z = 0) = F_0(x, y)$ .  $x$  and  $y$  are the downwind  
862 and crosswind distances (m) from the point where the  
863 measurements are taken, respectively.

$$F(x, y, z_m) = \int_{-\infty}^{\infty} \int_{-\infty}^x F_0(x', y') f(x - x', y - y', z_m) dx' dy' \quad (24)$$

864  
865  
866 As already mentioned, each point is weighted according  
867 to the spatial weighting function of the LAS (Meijninger  
868 2003): Where  $F_{LAS}(x, y, Z_{LAS})$  is the LAS footprint, and  
869  $F(x, y, Z_{LAS})$  is the flux footprint for a point located at  $d$   
870 distance from the transmitter.  $G(d)$  is the scintillometer path-  
871 weighting function for the position located at  $d$  distance.

$$F_{LAS}(x, y, Z_{LAS}) = \sum_{i=1}^N F(x, y, Z_{LAS}) G(d) \quad (25)$$

## 872 Appendix 2

873  
874  
875 The partitioning of LST into its soil and vegetation compo-  
876 nents is based on the LST and  $fc$  within the polygon (Fig.  
877 14) to determine one of the temperature components  $T_v$  or  
878  $T_s$  as follow:

879 For a given data point located in the evaporation-con-  
880 trolled zone,  $T_v$  computed as:

$$T_v = \frac{T_{v_{\max}} + T_{v_{\min}}}{2} \quad (26)$$

881  
882  
883 For a given data point located in the transpiration-con-  
884 trolled zone,  $T_s$  computed as:

$$T_s = \frac{T_{s_{\max}} + T_{s_{\min}}}{2} \quad (27)$$

887 For a given data point located in the stressed mixed sur-  
888 face zone,  $T_v$  computed as:

$$889 \quad T = \frac{LST - T_{s_{\max}}}{fc} + T_{s_{\max}} \quad (28)$$

$$891 \quad T_v = \frac{T_{v_{\max}} + T}{2} \quad (29)$$

893 For a given data point located in the unstressed mixed  
894 zone,  $T_v$  computed as:

$$895 \quad T = \frac{LST - T_{s_{\min}}}{fc} + T_{s_{\min}} \quad (30)$$

$$897 \quad T_v = \frac{T_{v_{\max}} + T}{2} \quad (31)$$

899 Then, the other component  $T_v$  or  $T_s$  was derived based on  
900 a linear decomposition of the LST in its vegetation and soil  
901 components as follows:

$$902 \quad LST = ((1 - fc)T_s^4 + fcT_v^4)^{1/4} \quad (32)$$

904 In what follows,  $fc$  is derived from Landsat NDVI using  
905 the following equation:

$$906 \quad fc = 1 - e^{-0.5 \times LAI} \quad (33)$$

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