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From real soils to 3D-printed soils: reproduction of complex pore network at the real size in a silty-loam soil

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7

8 Abstract

Pore complexity and micro-heterogeneity are pivotal in characterizing biogeochemical processes in 9 soils. Recent advances in X-ray computed microtomography (microCT) allow the 3D soil 10 morphology characterization of undisturbed samples, although its geometrical reproduction at very 11 small spatial scales is still challenging. Here, by combining X-ray microCT with 3D multijet 12 printing technology, we aimed to evaluate the reproducibility of 3D-printing soil structures at the 13 14 original scale with a resolution of 80 µm and compare the hydraulic properties of original soil samples with those obtained from the soil-like prototypes. Results showed that soil-like prototypes 15 16 were similar to the original samples in terms of total porosity and pore shape. By contrast the pore 17 connectivity was reduced by the incomplete wax removal from pore cavities after the 3D printing 18 procedure. Encouraging results were also obtained in terms of hydraulic conductivity since 19 measurements were successfully conducted on five out of six samples, showing positive correlation 20 with experimental data. We are confident that future developments of 3D-printing technologies and 21 of their combination with microCT will help to further the understanding of soil micro-22 heterogeneity and its effects on soil-water dynamics.

24 **1. INTRODUCTION**

25 The processes that form porous media lead to highly heterogeneous three-dimensional structures, forcing scientists to adopt models for reproducing the reality. This is the case for soil physics, which 26 27 has its foundations laid on the capillary bundle model (Hunt et al., 2013). Water flow is still 28 commonly conceptualized as a 2D bundle of cylindrical tubes passing through the soil only in the vertical direction, trivializing the natural complexity of a soil. As a result, derived models such as 29 30 those of water conductivity (Burdine, 1953; Mualem, 1976) introduced empirical adjustments (e.g. a tortuosity factor) to compensate for fundamental errors in the conceptual model (Hunt et al., 31 2013). The simplification of reality in one-dimensional or two-dimensional models was supported 32 by the inability to see and understand the 3D structure and its interactions with biota due to its 33 34 opaque nature (Feeney et al., 2006). However, recent advanced technologies have provided a vast 35 amount of data and their assimilation in more complex models that have partly superseded the use 36 of reduction methods (Ahuja et al., 2006). The first steps for creating real-world situations in soil science used 3D random network models (e.g., Rajaram et al., 1997; Peat et al., 2000) that 37 mimicked the soil complexity and dynamics in a three-dimensional space. In spite of their overall 38 improvement in the understanding of matrix flow and transport of solutes, these models had two 39 main limitations: a) computing limitations make some structural simplification unavoidable and b) 40 the soil has such structural complexity that a reliable estimate of a representative elementary 41 volume is difficult to quantify (Peat et al., 2000), as for most of the models. Lately, non-invasive 42 imaging approaches have gained attention as they provide the opportunity to examine soil-water 43 interactions from direct observations at the microscale. For example, the soil physical and chemical 44 processes were replicated using high-tech materials with a refractive index similar to water, 45 allowing the use of 3D optical microscopy in a transparent-reconstructed medium for the 46 47 visualization of biophysical processes. Controlled experiments of how pore channels can influence

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the biological and hydraulic dynamics can be realized, although the reconstructed medium is only
partially reproducible because it is composed of single incoherent particles (Downie et al., 2012).

50 Impressive developments and insights into porous media research have also been provided by X-ray computed microtomography (microCT) that allows microscopic visualization of the spatial 51 52 arrangement of complex structures (Cnudde and Boone, 2013). For the first time it became possible to investigate the interior of an object in a non-destructive way and to extract qualitative and 53 54 quantitative information of multiphase porous materials (e.g., Tippkoetter et al., 2009; Mooney et al., 2012). In this context "digital rock physics", i.e. the study of pore scale processes by the use of 55 digital imaging and modelling, has expanded enormously the understanding of single and 56 multiphase flow dynamics (Blunt et al., 2013). 57

58 Only recently 3D-printers have gained attention in the design of niche products, prototypes and onetime creations (e.g., Rangel et al., 2013), although the technology is 30-years old. This technology 59 has been proposed in research as a tool to integrate virtual microCT information with real building 60 models. In fact, the combination of such techniques make it possible to reconstruct complex 61 microcosms with the heterogeneity discovered with microCT at a resolution of few micrometers, 62 63 providing the opportunity to isolate the physical and chemical aspects that govern the biogeochemical and microbial processes in the soil (Otten et al., 2012; Ju et al., 2014; Bacher et al., 64 65 2015; Ringeisen et al., 2015). Nowadays, with 3D printing the diversified geometry encountered in a soil can be replicated at a resolution of tends of micrometers. Several materials can be used 66 67 including plastics, resins, ceramics and metals.

Despite large uncertainties persisting about soil microscale heterogeneity and its effects on the macroscopic dynamics (Baveye et al., 2011), so far few have tried to combine high-resolution 3D imaging and printing technology to improve knowledge in soil science. In this study we combined 3D printing technology with X-ray microCT in an attempt to reconstruct the 3D complexity of the soil structure in a soil-derived model at the same spatial scale as the original one and test somehydraulic properties.

74

75 2. MATERIAL AND METHODS

76 *Experimental design and soil sampling*

The soil samples come from a long-term experiment established in 1962 at the experimental farm of 77 78 the University of Padova (Italy). The soil (Table 1) is Fluvi-Calcaric Cambisol (CMcf), silty loam (FAO-UNESCO, 1990). This work considered soil samples from a long-term trial that compares 79 two treatments: farmyard manure at 60 t ha^{-1} y⁻¹ (hereafter labelled "M") and a no fertilization 80 control (hereafter labelled "C") on a continuous maize crop system. The same type of tillage has 81 82 been used for both treatments, with autumn plowing and subsequent cultivations prior to sowing the main crop. The experimental layout is a randomized block with three replicates, on plots of 7.8×6 83 m. Further details on experimental design are extensively reported in the literature (e.g., Morari et 84 al., 2006). A total of six undisturbed soil cores (5 cm diameter, 6 cm length) were collected in 85 August 2010 (Fig. 1, step A), at the end of the maize season, from the topsoil (5 to 20 cm depth) in 86 polymethylmethacrylate (PMMA) cylinders using a manual hydraulic core sampler (Eijkelkamp, 87 The Netherlands). Cores were stored at 5 °C until analysis. 88

89

90 *MicroCT soil scanning and image processing*

91 The pore structure of soil cores, labelled " M_{soil} " and " C_{soil} " for farmyard manure and no 92 fertilization control, respectively (Fig. 1, step B) was sampled using X-ray computed 93 microtomography (microCT). In order to allow the scanning of the whole soil core at a fine 94 resolution, samples were analyzed at the "3S-R" facility in Grenoble (http://www.3sr-grenoble.fr//)

at a spatial resolution of 40 µm. Setting parameters were 100 kV, 300 µA and projections were 95 collected during a 360° sample rotation at 0.3° angular incremental step. Each projection was the 96 mean of 10 acquisitions and scan frequency was 7 images s⁻¹. Beam hardening artifacts were 97 minimized during data acquisition using a 0.5 mm Al filter. In order to avoid pixel misclassification 98 99 that might occur during projection measurements due to scattered radiation, nonlinearity of data 100 acquisition systems, partial volume effects etc. (Hsieh, 2009), 2D projections were resized after 101 acquisition using a mean filter by a two-pixel factor along the vertical and horizontal axis. As a 102 result, the reconstructed images had a coarser resolution than that of acquisition (i.e. 80 µm). 103 Resized projections were finally reconstructed using the dedicated software DigiCT 1.1 (Digisens, France) to obtain a stack of about 750 2D slices in 32-bit depth. 32-bit images were later converted 104 105 into 8-bit depth.

106 The digital image processing and analysis of soil samples, conducted with the public domain image 107 processing ImageJ (Vs. 1.45, National Institute of Health, http://rsb.info.nih.gov/ij), has already 108 been reported in (Dal Ferro et al., 2013). Briefly, a cylindrical volume of interest with a diameter of 600 pixels and composed of 600 slices (4.8 cm height \times 4.8 cm diameter) was selected in order to 109 110 exclude the PMMA sample holder. Slices were segmented using a global-threshold value based on 111 the histogram greyscale that was determined by the maximum entropy threshold algorithm. The 112 threshold value was selected where the inter-class entropy was maximized (Luo et al., 2010). 8-113 connectivity, a mathematical morphology closing operator (Serra, 1982), was applied to the binary 114 images to fill misclassified pixels inside the pores as well as to maintain pore connections (Mooney et al., 2006). Successively, the one interconnected pore network (infinite cluster) that contained 115 116 most of the porosity within each stack was extracted and analyzed with CTAn software v. 1.12.0.0 (Bruker micro-CT, Kontich, Belgium) as this pore space was the only one to show continuity 117 118 between the top and bottom of the soil cores. Although more connections between pores were likely 119 present within the soil cores, microCT imaging provided only connections larger than the resolution

limits, restricting our analysis to the soil macroporosity. A description of the soil morphological
parameters as a result of microCT scanning has already been reported in Dal Ferro et al. (2015)
(Table 1).

123

124 *3D mesh generation*

125 A surface mesh model for each sample (3 replicates \times 2 treatments) was extracted from the one 126 interconnected pore network that was identified from the microCT stacks using the free software 127 InVesalius 3.0 (CTI, Campinas, São Paulo, Brazil) (Fig. 1, step G). The created model was then exported in the geometrical stereolithography file format encoded in Standard Tessellation 128 129 Language (STL). The reconstructed STL model, composed of 10 to 30 million triangles depending 130 on the complexity of the pore network, was visualized with the open-source software MeshLab 131 v.1.3.2 (STI-CNR, Rome, Italy; http://meshlab.sourceforge.net/) in order to assess the continuity of 132 pore connections along the vertical axis and successively simplified to a polygonal mesh that 133 consisted of up to 10 million triangles. In order to compare the microCT imaging from the original samples with the 3D-printed prototypes from the STL model, one of the three replicate microCT 134 135 stacks was selected for both "M" and "C". Afterwards a volume of interest, corresponding to a cylinder of 300 pixels height \times 300 pixels of diameter (Fig. 1, step C), was extracted by both 136 137 samples (2.4 cm high \times 2.4 cm diameter). InVesalius 3.0 was used to obtain a polygonal mesh model, from which a STL file was exported (Fig. 1, step D). MeshLab v.1.3.2 was used to simplify 138 139 the polygonal mesh at two levels of detail, corresponding to 500 thousand (500k) and 10 million (10M) triangles respectively. Each model was 3D-printed twice (Fig. 1, step E), resulting in a total 140 141 of eight models (2 soil samples \times 2 generated meshes \times 2 replicate printings). All the closed pores, 142 i.e. the pores that had no connection to the space outside, were then digitally removed from the 143 stacks since they cannot contribute to flow properties of the model.

145 *3D printing*

146 Lastly, 14 polygonal meshes (6 cylinders, 4.8 cm $h \times 4.8$ cm diameter; 8 cylindrical subsamples, 2.4 cm h \times 2.4 cm diameter) were built with a commercial 3D printer. The printer (ProJet 3510 HD, 3D 147 148 Systems, http://www.3dsystems.com/) was selected as it provided a fast prototype reconstruction with high resolution and available at a relatively low price (few hundred €). The 3D structure was 149 printed with resin whose exact composition is proprietary but approximately contained an organic 150 mixture of: ethoxylated bisphenol A diacrylate (15-35%), urethane acrylate oligomers (20-40 %), 151 152 tripropyleneglycol diacrylate (1.5-3%) (Visijet Crystal, EX 200 Plastic material, Safety Data Sheet, http://www.3dsystems.com). The 3D printer has a multijet printing technology, i.e. an inkjet 153 printing process that deposits either photocurable plastic resin or casting wax materials layer by 154 155 layer, with a spatial resolution of 29 μ m and a declared accuracy of 25-50 μ m, depending on 156 building parameters and prototype size and geometry. The final result was a set of solid prototypes 157 whose pores were filled with paraffin wax (the contact angle between water and wax, measured 158 with a goniometer, was 120°), while the soil matrix was composed of the resin. The contact angle between the pure resin (cleaned of any wax) and the water, measured with a contact angle 159 goniometer, was 69°. 160

161

162 *Wax removal procedure*

Wax removal is crucial in order to empty the pores and accurately replicate the complex geometry of the soil samples. Ultrasonication in oil at a temperature of 60 °C and 60 Hz for 24 h and oven drying at 60 °C until stabilized weight (*ca.* four days) were adopted as possible procedures to empty the pores. Alternative methods were considered: the use of xylene or vapor steam cleaning would have dissolved the wax, although it would have probably corrupted the solid pore surface, while alternative printing technologies without the use of wax as a physical support during 3d printing were not feasible. As a result, we adopted a simple and relatively low-cost combination between 3Dprinting technology and cleaning procedure.

171

172 *3D prototypes scanning, image reconstruction and analysis*

The resulting prototypes from the sub-volume of the samples (i.e. "M_{small}" and "C_{small}" at a detail of 173 500 thousand and 10 million triangles) were finally subjected to X-ray microCT scanning (Fig. 1, 174 175 step F) in order to assess: a) the reproducibility and reliability of the 3D printing process; b) the smoothing effect of polygon reduction on the generated 3D structure; c) efficacy of the cleaning 176 177 procedure to remove the wax from the pores. Prototypes were analyzed with a Skyscan 1172 X-ray microtomography (Bruker micro-CT, Kontich, Belgium) at the University of Padova since lower 178 energy than those used for scanning the whole soil sample was required to penetrate the specimen. 179 180 Setting parameters were 40 kV, 250 µA and projections were collected during a 180° sample rotation at 0.25° angular incremental step. Each projection was the mean of eight acquisitions and 181 scan frequency was 1.33 images s⁻¹. Beam hardening artifacts were minimized during data 182 acquisition using a 0.5 mm Al filter. The spatial resolution was 27 µm. In order to avoid pixel 183 184 misclassification that might occur during image acquisition (Hsieh, 2009), projections were resized 185 after acquisition using a mean filter by a two-pixel factor along the vertical and horizontal axis. As a result, the reconstructed images had a final resolution twice that of acquisition (i.e. 54 µm). Resized 186 projections were reconstructed using the dedicated software NRecon v. 1.6.9.4 provided by Bruker 187 micro-CT to obtain a stack of about 450 2D slices in 16-bit depth. 16-bit images were later 188 converted into 8-bit depth. 189

Prototype matrix, wax and void phases were easily visualized and binarized with a single threshold
level. 8-connectivity was applied to the binary images to fill misclassified pixels inside the pores as
well as to maintain pore connections (Mooney et al., 2006). MicroCT porosity (m³ m⁻³), pore size

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distribution and open porosity (%), pore surface to volume ratio (μ m⁻¹), 3D fractal dimension and Euler number (mm⁻³) were estimated from each binarized stack using CTAn and compared with soil parameters obtained from the original sub-volume samples.

196

197 *Hydraulic conductivity test on 3D-printed prototypes*

Saturated hydraulic conductivity (Ks-large) measurements were conducted on the large prototypes 198 (" M_{large} " and " C_{large} ", 4.8 cm high \times 4.8 cm diameter) (Fig. 1, step H) by using a laboratory 199 200 permeameter (Eijkelkamp, The Netherlands) that was adjusted to the size of the samples by using a 201 gasket whose thickness created a seal at the interface between the prototype and the sample holder. K_{s-large} was determined with both constant and variable head method, according to the hydraulic 202 properties of the medium. As a rule of thumb, K_{s-large} values greater than 5.8 10⁻⁶ m s⁻¹ were easily 203 204 determined by the constant head method, while the falling head method was conducted at smaller K_{s-large} values. Before conducting the analysis and to ensure that water flowed only vertically from 205 206 the top to the bottom of the prototypes, avoiding the loss of water from lateral pores, samples were firstly sealed with a plastic tape and successively coated with a layer of melted wax. As a result, it 207 208 was ensured the complete sealing of the samples avoiding the lateral occlusion of interior pores. 209 Successively samples were freely upward saturated at atmospheric pressure (water bath reached ³/₄ of sample height) using de-aerated water, then subjected to 0.6 10⁻⁵ Pa to completely de-aerate them 210 211 and saturated again as above.

212

213 *Hydraulic conductivity test on original samples*

Saturated water conductivity on soil-like prototypes was compared with water flow calculated on the original soil samples and already proposed in (Dal Ferro et al., 2015). As a result, original samples were subjected to saturated water conductivity analyses (K_{s-soil}, m s⁻¹) using the constant 9 5585 Guilford Rd., Madison WI 53711 head or falling head method, depending on the soil properties and range of K_{s-soil} that can be measured (Reynolds et al., 2002). In addition, the microCT imaging dataset of the original samples (scanned at the "3S-R" facility in Grenoble) was used to calculate water conductivity on the one interconnected pore cluster (K_{Morph} , m s⁻¹) by using a morphologic approach as proposed by (Elliot et al., 2010). Briefly, the model consisted of combining three dimensional pore shape parameters with pore volume and using a modified Poiseuille equation as follows:

223
$$Q = \frac{\pi R^4 \Delta P}{8L_c \nu} , \qquad [1]$$

where *R* is pore radius, *v* is the viscosity of water at room temperature, ΔP is the change in hydrostatic pressure and L_c is the pore length, depending on pore shape characteristics.

Lastly, rearrangement of Darcy's law allowed the K_{Morph} estimation for the extracted pore network:

227
$$K = \frac{QL}{A\Delta P},$$
 [2]

where *A* is the cross-sectional area of the sample and *L* is the sample length. A detailed description of the methods and results for the soils proposed here can be found in Dal Ferro et al. (2015).

230

3. RESULTS

232 *Soil volume and prototype measurements*

Ultrasonication in oil was only partially able to remove the wax from pores, while the subsequent oven drying at 60 °C was able to remove most of it (Fig. 2). A further increase in temperature was not possible because, according to the manufacturer, it would have weakened the resin structure or melted part of it. As a result, the combination of both techniques was used as the best procedure currently available to successfully empty the open pores as well as maintain the solid structure.

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However, the continuing advances in 3D-printing technology and the use of heat-resistant materialswill allow the full removal of the support material (e.g. by evaporation).

240 Soil porosity of sub-volumes scanned with microCT (" M_{soil} " and " C_{soil} " 2.4 cm high \times 2.4 cm 241 diameter) was entirely connected to the space outside the soil matrix (open pores/total porosity = 100%), but highly different between "M_{soil}" (0.114) and "C_{soil}" (0.036) (Table 2). The open pores of 242 "M_{small}" prototypes were slightly lower than porosity detected by microCT, with negligible changes 243 244 between 500 thousand (500k) and 10 million (10M) triangle meshes. Indeed, only 2.4% of microCT porosity (0.109 and 0.110 in 500k and 10M, respectively) was confined within the solid phase 245 (Table 2). By contrast, the "C_{small}" prototypes showed a consistent increase of confined pores with 246 247 respect to the total ones, ranging from 15.1% in the 500k to 18.4% in the 10M meshes, on average. 248 As a result, the " C_{soil} " porosity (0.036) was slightly greater than " C_{small} " built both from 500 249 thousand (0.024) and 10 million (0.027) triangle meshes respectively.

250 Pore size distribution (PSD) curves (Fig. 4), measured on microCT images in volumetric terms 251 according to the medial-axes determination and sphere-fitting measurement (Remy and Thiel, 2002), were distributed differently between "M" and "C". In "M" the most frequent pore classes 252 253 were distributed between 240 µm and 560 µm diameter, while they were shifted towards smaller 254 pores in "C", ranging between 160 µm and 440 µm. Comparable data were found between PSD 255 prototype classes, in both "M" and "C", with negligible variations between replicates and meshes. 256 By contrast, a sharp increase of the small pores was observed in the original samples with respect to 257 the prototypes: this was particularly clear for pore classes smaller than 800 μ m and 490 μ m in "M_{soil}" and "C_{soil}", where the integral of the PSD differences was around 30% and 10% of microCT 258 259 porosity, respectively. Finally, it was noticed that some pores were still filled with wax despite its 260 melting and removal with ultrasonication and oven drying (Fig. 3). In particular, wax most resided 261 in thin throats ($\leq 200 \,\mu m$, on average) between largest cavities, leading to their disconnection and 262 thus increasing both the average size of empty pores and the number of isolated ones.

Pore morphological features (Table 2), estimated by means of pore surface/volume ratio (μm^{-1}) , 263 264 Euler number (i.e. an indicator of pore connectivity, where the greater is the value, the lower is the pore connectivity; mm⁻³) (Vogel et al., 2010) and 3D fractal dimension (box-counting method) 265 (Perret et al., 2003), emphasized the self-similarity between the prototypes that were generated by 266 the same original sub-volume. For instance, the pore surface/volume ratio was 0.007 μ m⁻¹ in 267 "M_{small}" prototypes as characterized by different meshes (500k and 10M triangles), while the fractal 268 dimension (2.42 and 2.25 in the original "M_{soil}" and "C_{soil}", respectively) ranged in "M_{small}" 269 between 2.10 (500k triangles) and 2.62 (10M triangles) and in "C_{small}" between 2.38 (500k 270 triangles) and 2.55 (10M triangles). Only the Euler number parameter, particularly in "M_{small}" and 271 "C_{small}" built from 500k triangle meshes, showed high variability between the prototypes (Table 2). 272

273

274 Experimental saturated hydraulic conductivity measurements on large prototypes

Experimental saturated hydraulic conductivity ($K_{s-large}$) data were obtained on five of the six 275 reconstructed large prototypes (" M_{large} " and " C_{large} " 4.8 cm high × 4.8 cm diameter, an example is 276 reported in Fig. 5) since water did not flow through one of the "Clarge" samples (Table 3). K_{s-large} 277 was generally higher in "M" (18.5 m s⁻¹, on average) than "C" (0.035 m s⁻¹, on average), ranging 278 between a minimum of 0.023 m s⁻¹ observed in "C" and a maximum of 13.5 m s⁻¹ in "M. The water 279 flow measurements on the prototypes were generally greater (7.65 10^{-5} m s⁻¹, on average) than those 280 measured ($K_{s-soil} = 3.59 \ 10^{-6}$, on average) and modelled ($K_{Morph} = 1.91 \ 10^{-6} \ m \ s^{-1}$) on the original soil 281 samples (Table 3) (Dal Ferro et al., 2015). Finally, positive correlations were observed between 282 soil-like K_{s-large} values and both K_{s-soil} ($R^2 = 0.69$) and K_{Morph} ($R^2 = 0.93$, Fig. 6). 283

284

285 4. DISCUSSION

286 The comparison between morphological characteristics of replicated small prototypes ("M_{small}" and "C_{small}") showed that 3D printing technology was able to retain the basic features of the macropore 287 network. More specifically, the pore size and shape characteristics of the largest pores was easily 288 289 visualized on the microCT imaging (Fig. 3), highlighting the similarity between reconstructed 290 models. Moreover, introducing some smoothing of the surface walls by the simplification of the 291 mesh (500 thousand vs. 10 million triangles) did not show significant changes between macropore 292 characteristics. In particular, the "M" microCT porosity and pore surface/volume ratio had a 293 coefficient of variation of 3.6% and 4.8%, respectively. These results were supported by others: 294 Otten et al. (2012) reported a very high reproducibility of twelve prototypes since the measured 295 porosity (0.66) was characterized by a very low coefficient of variation (3.36%), although their soil-296 like prototypes were scaled up three times with respect to the original size of the soil samples. By 297 contrast, our prototypes were reconstructed at the real size, although the soil microscale 298 heterogeneity that was provided by the fine silt and clay particles could not be faithfully reproduced due to the microCT soil scanning (40 μ m) and 3D printing resolution limits (29 μ m). 299

The successful reproduction of generated "M_{small}" prototypes (Fig. 1, step E) was partly reappraised 300 301 by evaluating the pore morphological characteristics in detail (Table 2). In fact, the pore structure parameters varied between the reconstructed models, especially in the "Csmall" prototypes. For 302 303 instance, the coefficient of variation of total porosity was 11.5% in the "C_{small}" prototypes, 304 increasing to 63% in the Euler number. Nevertheless, it is worth noticing that the microCT scanning 305 of small prototypes (Fig. 1, step F) was performed at a resolution (27 μ m) that was finer than that 306 used during the 3D-printing (29 μ m, \pm 50 μ m), emphasizing the systematic errors during the model 307 building process. As a result, the mismatch observed between soil samples ("M_{soil}" and "C_{soil}") and prototypes ("M_{small}" and "C_{small}") structures were the result of the combined effect between: a) soil 308 309 digital imaging due to microCT scanning; b) inaccuracy during the 3D printing process; c) 310 prototype digital imaging due to microCT scanning. Furthermore, the 3D mesh generation created 311 distorted elements from the voxel-based microCT volumes, although the negligible variations 312 between small prototypes as printed from 500 thousand and 10 million triangles suggested their minor role during the prototypes production. Moreover, the partial effectiveness of wax removal 313 from the macropores (Fig. 3), quantified at around 2.4% ("M_{small}") and 16.7% ("C_{small}") of microCT 314 315 porosity, increased the uncertainty on the pore quantity and morphology. Finally, the biggest 316 differences were observed in terms of Euler number, showing its ability to identify slight structure 317 changes between replicated prototypes. The wax entrapped in the voids created a discontinuity 318 between adjacent pores by modifying the degree of connection of the macropore network and partly isolating them from the space outside the solid matrix. As a result, the soil volumes ("M_{soil}" and 319 "C_{soil}") generally had both a higher microCT total porosity and a lower Euler number (i.e. more 320 321 connections) than the reconstructed prototypes (Table 2). As suggested by the pore size distribution 322 analysis, the wax was easily removed from the largest pores, while it consistently remained in the 323 smallest ones (Fig. 4). Finally, a mismatch between soil and soil-like porosity was probably introduced during microCT soil analysis and the following mesh generation. Indeed microCT 324 325 imaging was composed of cubic voxels while polygonal mesh comprised a surface triangulation, avoiding their full overlap. 326

327 In spite of the difficulty in totally cleaning the wax from the macropores, measurements of saturated 328 hydraulic conductivity were successfully conducted on five of the six large prototypes. Only the saturated conductivity measurement on one "Clarge" prototype failed. Since one of the "Clarge" soil-329 330 derived model was characterized by the lowest total porosity (0.015), most likely the entrapped wax occluded the scarce conductive pores within the whole prototype and prevented flow. Water flow 331 332 measurements, calculated through the one interconnected macropore network that spanned the sample, were highly correlated with properties calculated on the original samples (K_{s-soil}) and 333 334 particularly with those modelled (K_{Morph}) on the same pore network (Fig. 6) (Dal Ferro et al., 2015). 335 Nevertheless, K_{s-large} had higher values than K_{s-soil} and K_{Morph} by at least one order of magnitude in 336 the "M" treatment (Table 3), although the total porosity had been reduced with respect to the soil 337 sample ones in two ways: a) the prototypes were reconstructed on the basis of digital imaging from 338 microCT scanning that performed at a resolution that excluded all the small connections between 339 the largest pores and decreased the adsorption along the macropore walls; b) part of microCT 340 porosity was probably still filled with wax during K_{s-large} measurements, reducing the water flow 341 capacity of the porous medium. These results suggested the major role of conducting macropores on 342 water flow dynamics (Jarvis, 2007), although the undetected and unprinted micropores $< 80 \ \mu m$ might have partially increased K_{s-large} to approach the experimental K_{s-soil} (Elliot et al., 2010), 343 344 particularly when the soil structure was largely composed of thin pores and microcracks are often 345 insufficiently imaged with microCT and thus underrepresented (i.e. in the control samples), 346 especially in the vicinity of grain contacts (Andrä et al., 2013). Some smoothing of the pore 347 surfaces, introduced during the prototype generation, decreased the friction factor between the 348 liquid and solid phases with respect to the original samples, as was shown by the results of pore 349 surface/volume ratio (Table 2). This would have reduced the pressure drop (Kumar et al., 2011) at 350 high K_{s-large} values, obeying the dynamics on the viscous forces as described in the Stokes 351 equations, while with low water velocity the difference between K_{s-large} and K_{s-soil} and K_{Morph} was 352 strongly reduced. By contrast, the contact angle between the water and the solid walls (69°) was 353 only a minor factor for influencing the water movement, although it is reasonable that, despite the 354 emptying procedure, the pores were still coated with wax that would have induced fluid slip for 355 water flowing over a hydrophobic surface (Tretheway and Meinhart, 2002).

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357 **5. CONCLUSIONS**

Integrating X-ray microtomography and 3D printing technology is feasible in soil science at the microscale and provides great opportunities to better understand the role of micro-heterogeneity in the soil-water dynamics. In particular, soil-like prototypes were built with relatively large 15 361 replicability and similarity to the original ones at the actual size, with a resolution of 80 μ m. 362 Moreover, the mesh simplification (from 100 million to 500 thousand triangles) did not reveal significant differences between prototypes. By contrast, the full wax removal from the pores was 363 364 not completely solved as it limited the pore connectivity and increased the surface smoothing. 365 Nevertheless, water conductivity was successfully performed on five of the six large prototypes, 366 showing a strong correlation with experimental and modelled data from the original soil samples. 367 The comparison between K_{s-large} (i.e. on prototypes) and K_{Morph} (morphologic model) data, 368 performed on the same porous systems, highlighted the major role of the macropore surface 369 smoothing and the hydrophobic nature of wax. In particular, an increase of fluid slip and consequently of water velocity at laminar flow was observed for $K_{s-large} \ge 10^{-5} \text{ m s}^{-1}$, while it was 370 consistently reduced at lower values. By contrast, the detection of micropores $< 80 \ \mu m$ would have 371 372 approached the K_{s-large} values to reach the experimental ones (K_{s-soil}), especially at low water 373 velocities. In order to promote a broad application of 3D prototypes in the hydrological research, future application of 3D printing technology should address many technological challenges. In fact 374 375 a higher microCT scanning and 3D-printed resolution will favor the representation of the soil pore 376 system at the nanoscale and its heterogeneity. Moreover the use of soil-like materials will be able to 377 model the physical-chemical interaction between water and the pore surface. Nevertheless, even at 378 this stage, our work suggests as 3D printing technology can represent a breakthrough technology for 379 the study of soil structure and its interaction with biogeochemical processes.

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476 **Captions of figures**

477 **Figure 1** Outline of steps used to obtain soil-like prototypes and sample measurements.

Figure 2 2D slices from microCT imaging (M = farmyard manure; C = control) of original soil samples (A1, B1) and soil-like prototypes after the wax removal procedure with ultrasonication (A2, A3, B2, B3) and oven drying (A4, B4).

Figure 3 2D slices from microCT imaging of original soil samples (A1, B1) and soil-like prototypes (M = farmyard manure; C = control). Prototypes were obtained in duplicate from a polygonal mesh composed of both 500 thousand (500k; A2, A5, B2, B5) and 10 million (10M; A3, A6, B3, B6) triangles. Grayscale images are composed of empty pores (black objects) and solid material (gray objects). Binary images are composed of empty pores (white) and solid material (black).

- **Figure 4** Pore size distribution estimated by means of X-ray microCT on original soil samples (" M_{soil} and " C_{soil} ") and on soil-like prototypes (" M_{small} " and " C_{small} ") from 3D printing at different mesh accuracy (500k = 500 thousand triangles; 10M = ten million triangles).
- 490 **Figure 5** 3D representations of a large soil sample (farmyard manure treatment) as a result of X-ray
- 491 microCT analysis (A, C; spatial resolution of 40 μ m) and pictures of its 3D-printed copy (B, D;
- 492 spatial resolution of 29 μ m).
- 493 Figure 6 Relationship between saturated water conductivities estimated on soil-like prototypes (K_{s} -
- 494 $_{\text{large}}$, m s⁻¹) and on the original soil samples by means of (A) experimental (K_{s-soil}, m s⁻¹) and (B)
- 495 modelling (K_{Morph} , m s⁻¹) approach.

496	Table 1 Texture and microCT pore morphological parameters of original soil cores (4.8 cm high × 4.8 cm diameter). Standard error values are
497	reported in brackets.

			Soil physi	cal proper	ties	MicroCT parameters			
ID	Replicate	Sand (%)	Silt (%)	Clay (%)	Total porosity ^a (m ³ m ⁻³)	MicroCT porosity (m ³ m ⁻³)	Mean pore diameter ^b (µm)	Pore surface/volume (μm^{-1})	Euler number (mm ⁻³)
М	1	32.1	63.3	4.7	0.490	0.086	783.74	0.008	0.31
М	2	32.0	63.3	4.7	0.461	0.102	530.24	0.011	1.09
М	3	30.0	65.0	5.0	0.476	0.045	883.97	0.009	0.16
Aver	age	31.4(0.7)	63.9(0.6)	4.8(0.1)	0.476(0.008)	0.078(0.017)	732.65(105.26)	0.009(0.001)	0.52(0.29)
С	1	27.5	65.7	6.7	0.459	0.015	386.96	0.011	0.16
С	2	37.8	57.2	5.0	0.432	0.020	338.58	0.014	0.6
С	3	32.6	62.0	5.4	0.439	0.033	374.06	0.013	3.13
Aver	age	32.6(3.0)	61.6(2.5)	5.7(0.5	0.443(0.008)	0.023(0.005)	366.53(14.46)	0.013(0.001)	1.65(1.21)
^a Grav ^b Wei	vimetric meth ghted mean c	od with wa f soil pore s	ter saturati size distrib	on. ution.		64	0		

^aGravimetric method with water saturation. 498

^bWeighted mean of soil pore size distribution. 499

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501 **Table 2** 3D parameters from microCT scanning of original soil volumes (" M_{soil} " and " C_{soil} ") and soil-like prototypes (" M_{small} " and " C_{small} "). Soil and soil-like volumes were 2.4 cm high × 2.4 cm diameter. Standard error values are reported in brackets.

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ID	Sample scanned	Mesh ^a	MicroCT porosity (m ³ m ⁻³)	Open pores/total porosity (%)	Mean pore diameter ^b (µm)	Pore surface/volume (µm ⁻¹)	Euler number (mm ⁻³)	3D fractal dimension
M_{soil}	Soil	-	0.114	100.00	858.60	0.007	0.42	2.41
M _{small}	Prototype	500k	0.113	98.97	925.60	0.007	3.54	2.61
M _{small}	Prototype	500k	0.106	96.36	943.26	0.007	0.82	2.10
M_{small}	Prototype	10M	0.113	98.71	940.04	0.007	1.70	2.62
M_{small}	Prototype	10M	0.107	96.32	953.31	0.007	0.97	2.17
Average	Prototype	-	0.110 (0.002)	97.591(0.84)	940.55(6.62)	0.007(0.000)	1.758(0.72)	2.38(0.16)
C _{soil}	Soil	-	0.036	100.00	319.02	0.014	0.33	2.25
C _{small}	Prototype	500k	0.027	90.30	397.66	0.013	0.981	2.40
C _{small}	Prototype	500k	0.022	79.59	393.33	0.013	0.171	2.55
C _{small}	Prototype	10M	0.028	86.35	380.00	0.013	0.795	2.38
C_{small}	Prototype	10M	0.025	76.90	246.21	0.026	1.509	2.46
Average	Prototype	-	0.026(0.002)	83.28(3.54)	354.30(41.83)	0.016(0.004)	0.864(0.319)	2.45(0.04)

 a 500k = 500 thousand tringle mesh; 10M = 10 million triangle mesh.

⁵⁰⁵ ^bWeighted mean of soil-like prototypes pore size distribution.

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- **Table 3** Experimental saturated conductivity values ($K_{s-large}$, m s⁻¹) estimated on soil-like prototypes (" M_{large} " and " C_{large} ", 4.8 cm high × 4.8 cm diameter) and compared with experimental (K_{s-soil}) and modelled (K_{Morph}) ones on the original soil samples. Standard error values are reported in
- 510 brackets.

	ID	Replicate	$K_{s-large}$ (10 ⁻⁶ m s ⁻¹)	K_{s-soil}^{a} (10 ⁻⁶ m s ⁻¹)	K_{Morph}^{a} (10 ⁻⁶ m s ⁻¹)	
	М	1	134.94	6.31	5.17	
	М	2	19.46	2.41	4.13	
	Μ	3	30.50	3.41	1.74	
	Average		61.63 (36.79)	4.04 (1.17)	3.68 (1.02)	
	С	1	N/A	5.27	0.04	
	С	2	0.23	2.22	0.16	
	С	3	0.47	1.90	0.24	
	Average		0.35(0.12)	3.13(1.07)	0.15(0.06)	
512	^a data from	Dal Ferro e	t al. (2015).			
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Figure 1 Outline of steps used to obtain soil-like prototypes and sample measurements. 216 x 127 mm (300 x 300 DPI)







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Figure 3 2D slices from microCT imaging of original soil samples (A1, B1) and soil-like prototypes (M = farmyard manure; C = control). Prototypes were obtained in duplicate from a polygonal mesh composed of both 500 thousand (500k; A2, A5, B2, B5) and 10 million (10M; A3, A6, B3, B6) triangles. Grayscale images are composed of empty pores (black objects) and solid material (gray objects). Binary images are composed of empty pores (white) and solid material (black). 119x160mm (300 x 300 DPI)



Figure 4: Pore size distribution estimated by means of X-ray microCT on original soil samples ("Msoil and "Csoil") and on soil-like prototypes ("Msmall" and "Csmall") from 3D printing at different mesh accuracy (500k = 500 thousand triangles; 10M = ten million triangles). 169x197mm (300 x 300 DPI)



Figure 5: 3D representations of a large soil sample (farmyard manure treatment) as a result of X-ray microCT analysis (A, C; spatial resolution of 40 μm) and pictures of its 3D-printed copy (B, D; spatial resolution of 29 μm). 118x130mm (300 x 300 DPI)



Figure 6 Relationship between saturated water conductivities estimated on soil-like prototypes (Ks-large, m s-1) and on the original soil samples by means of (A) experimental (Ks-soil, m s-1) and (B) modelling (KMorph, m s-1) approach. 317x152mm (300 x 300 DPI)